

PCT

WORLD INTELLECTUAL PROPERTY ORGANIZATION
International Bureau



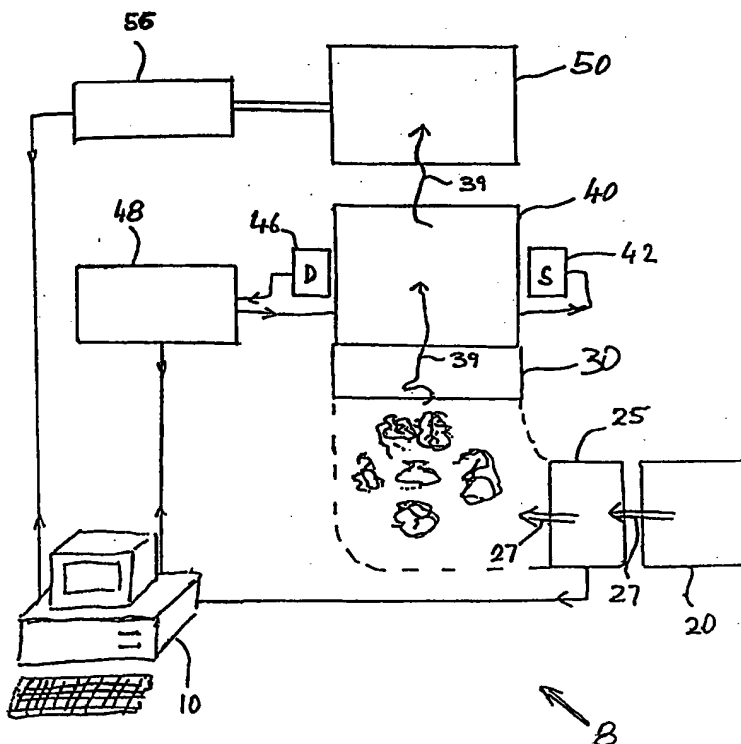
INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification ⁷ : C12Q 1/68		A1	(11) International Publication Number: WO 00/09757
			(43) International Publication Date: 24 February 2000 (24.02.00)
(21) International Application Number: PCT/US99/18438		(81) Designated States: AE, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CR, CU, CZ, DE, DK, DM, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, UA, UG, US, UZ, VN, YU, ZA, ZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SL, SZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).	
(22) International Filing Date: 13 August 1999 (13.08.99)			
(30) Priority Data: 60/096,544 13 August 1998 (13.08.98) US 60/120,414 14 February 1999 (14.02.99) US			
(71) Applicant (for all designated States except US): U.S. GENOMICS [US/US]; 9th floor, 8 Saint Mary's Street, Boston, MA 02215 (US).			
(72) Inventors; and (75) Inventors/Applicants (for US only): TEGENFELDT, Jonas, O. [-/US]; 28 Olden Lane, Princeton, NJ 08540 (US). AUSTIN, Robert, H. [-/US]; 135 Harris Road, Princeton, NJ 08544 (US). CHAN, Eugene, Y. [-/US]; Suite 4, 25 Beaver Place, Boston, MA 02108 (US).			
(74) Agent: LOCKHART, Helen, C.; Wolf, Greenfield & Sacks, P.C., 600 Atlantic Avenue, Boston, MA 02210 (US).			
		Published With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.	

(54) Title: OPTICALLY CHARACTERIZING POLYMERS

(57) Abstract

The invention is a system for optically characterizing polymers. Preferably the system is used to perform linear analysis of the polymers.



FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece	ML	Mali	TR	Turkey
BG	Bulgaria	HU	Hungary	MN	Mongolia	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MR	Mauritania	UA	Ukraine
BR	Brazil	IL	Israel	MW	Malawi	UG	Uganda
BY	Belarus	IS	Iceland	MX	Mexico	US	United States of America
CA	Canada	IT	Italy	NE	Niger	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NL	Netherlands	VN	Viet Nam
CG	Congo	KE	Kenya	NO	Norway	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NZ	New Zealand	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	PL	Poland		
CM	Cameroon	KR	Republic of Korea	PT	Portugal		
CN	China	KZ	Kazakhstan	RO	Romania		
CU	Cuba	LC	Saint Lucia	RU	Russian Federation		
CZ	Czech Republic	LI	Liechtenstein	SD	Sudan		
DE	Germany	LK	Sri Lanka	SE	Sweden		
DK	Denmark	LR	Liberia	SG	Singapore		
EE	Estonia						

OPTICALLY CHARACTERIZING POLYMERS

Field of the Invention

The present invention is directed to optical systems, methods and products for
5 analyzing polymers, and more particularly to optical systems, methods and products that
utilize highly localized optical radiation for characterizing individual units of polymers.

Background

This patent application claims priority from U.S. Provisional Application 60/096,544
10 filed on August 13, 1998, and U.S. Provisional Application 60/120,414 filed on February 14,
1999, both of which are incorporated by reference.

Cells have a complex microstructure that determine the functionality of the cell. Much
of the diversity associated with cellular structure and function is due to the ability of a cell to
assemble various building blocks into diverse chemical compounds. The cell accomplishes
15 this task by assembling polymers from a limited set of building blocks referred to as
monomers or units. The key to the diverse functionality of polymers is based in the primary
sequence of the monomers within the polymer and is integral to understanding the basis for
cellular function, such as why a cell differentiates in a particular manner or how a cell will
respond to treatment with a particular drug.

20 The ability to identify the structure of polymers by identifying their sequence of
monomers is integral to the understanding of each active component and the role that
component plays within a cell. By determining the sequences of polymers it is possible to
generate expression maps, to determine what proteins are expressed, to understand where
mutations occur in a disease state, and to determine whether a polysaccharide has better
25 function or loses function when a particular monomer is absent or mutated.

Expression maps relate to determining mRNA expression patterns. The need to
identify differentially expressed mRNAs is critical in the understanding of genetic
programming, both temporally and spatially. Different genes are turned on and off during the
temporal course of an organisms' life development, comprising embryonic, growth, and aging
30 stages. In addition to developmental changes, there are also temporal changes in response to
varying stimuli such as injury, drugs, foreign bodies, and stress. The ability to chart
expression changes for specific sets of cells in time either in response to stimuli or in growth

allows the generation of what are called temporal expression maps. On the other hand, there are also body expression maps, which include knowledge of differentially expressed genes for different tissues and cell types. Since generation of expression maps involve the sequencing and identification of cDNA or mRNA, more rapid sequencing necessarily means more rapid generation of multiple expression maps.

Currently, only 1% of the human genome and an even smaller amount of other genomes have been sequenced. In addition, only one very incomplete human body expression map using expressed sequence tags has been achieved (Adams et al., 1995). Current protocols for genomic sequencing are slow and involve laborious steps such as cloning, generation of genomic libraries, colony picking, and sequencing. The time to create even one partial genomic library is on the order of several months. Even after the establishment of libraries, there are time lags in the preparation of DNA for sequencing and the running of actual sequencing steps. Given the multiplicative effect of these unfavorable facts, it is evident that the sequencing of even one genome requires an enormous investment of money, time, and effort.

In general, DNA sequencing is performed using one of two methods. The first and more popular method is the dideoxy chain termination method described by Sanger et al. ("DNA sequencing with chain-terminating inhibitors," *Proc. Natl. Acad. Sci. USA.* 74:5463-7, 1977). This method involves the enzymatic synthesis of DNA molecules terminating in dideoxynucleotides. By using the four ddNTPs, a population of molecules terminating at each position of the target DNA can be synthesized. Subsequent analysis yields information on the length of the DNA molecules and the base at which each molecule terminates (either A, C, G, or T). With this information, the DNA sequence can be determined. The second method is Maxam and Gilbert sequencing (Maxam and Gilbert, "A new method for sequencing DNA," *Proc. Natl. Acad. Sci. USA.* 74:560-4, 1977), which uses chemical degradation to generate a population of molecules degraded at certain positions of the target DNA. With knowledge of the cleavage specificities of the chemical reactions and the lengths of the fragments, the DNA sequence is generated. Both methods rely on polyacrylamide gel electrophoresis and photographic visualization of the radioactive DNA fragments. Each process takes about 1-3 days. The Sanger sequencing reactions can only generate 300-800 bases in one run.

Sanger-based methods have been proposed to improve the output of sequence information. The Sanger-based methods include multiplex sequencing, capillary gel electrophoresis, and automated gel electrophoresis. Recently, there has also been increasing

interest in developing Sanger independent methods as well. Sanger independent methods use a completely different methodology to realize the base information. This category contains the most novel techniques, which include scanning electron microscopy (STM), mass spectrometry, enzymatic luminometric inorganic pyrophosphate detection assay (ELIDA) sequencing, exonuclease sequencing, and sequencing by hybridization.

Currently, automated gel electrophoresis is the most widely used method of large-scale sequencing. Automation requires reading of fluorescently labeled Sanger fragments in real time with a charge coupled device (CCD) detector. The four different dideoxy chain termination reactions are run with different labeled primers. The reaction mixtures are combined and co-electrophoresed down a slab of polyacrylamide. Using laser excitation at the end of the gel, the separated DNA fragments are resolved and the sequence determined by computer. Many automated machines are available commercially, each employing different detection methods and labeling schemes. The most efficient of these is the Applied Biosystems Model 377XL, which generates a maximum actual rate of 115,200 bases per day.

In the method of capillary gel-electrophoresis, reaction samples are analyzed by small diameter, gel-filled capillaries. The small diameter of the capillaries (50 μm) allows for efficient dissipation of heat generated during electrophoresis. Thus, high field strengths can be used without excessive Joule heating (400 V/m), lowering the separation time to about 20 minutes per reaction run. Not only are the bases separated more rapidly, there is also increased resolution over conventional gel electrophoresis. Furthermore, many capillaries are analyzed in parallel (Wooley and Mathies, "Ultra-high-speed DNA sequencing using capillary electrophoresis chips," *Anal. Chem.* 67:3676-3680, 1995), allowing amplification of base information generated (actual rate is equal to 200,000 bases/day). The main drawback is that there is not continuous loading of the capillaries since a new gel-filled capillary tube must be prepared for each reaction. Capillary gel electrophoresis machines have recently been commercialized.

Multiplex sequencing is a method which more efficiently uses electrophoretic gels (Church and Kieffer-Higgins, "Multiplex DNA sequencing," *Science*. 240:185-88, 1988). Sanger reaction samples are first tagged with unique oligomers and then up to 20 different samples are run on one lane of the electrophoretic gel. The samples are then blotted onto a membrane. The membrane is then sequentially probed with oligomers that correspond to the tags on the Sanger reaction samples. The membrane is washed and reprobed successively until the sequences of all 20 samples are determined. Even though there is a substantial

reduction in the number of gels run, the washing and hybridizing steps are as equally laborious as running electrophoretic gels. The actual sequencing rate is comparable to that of automated gel electrophoresis.

Sequencing by mass spectrometry was first introduced in the late 80's. Recent
5 developments in the field have allowed for better sequence determination (Crain,
MassSpectrom. Rev. 9:505-54, 1990; Little et al., *J. Am. Chem. Soc.* 116:4893-4897, 1994;
Keough et al., *Rapid Commun. Mass Spectrom.* 7:195-200, 1993; Smirnov et al., 1996). Mass
spectrometry sequencing first entails creating a population of nested DNA molecules that
10 differ in length by one base. Subsequent analysis of the fragments is performed by mass
spectrometry. In one example, an exonuclease is used to partially digest a 33-mer (Smirnov,
"Sequencing oligonucleotides by exonuclease digestion and delayed extraction matrix-
assisted laser desorption ionization time-of-flight mass spectrometry," *Anal. Biochem.* 238:19-
25, 1996). A population of molecules with similar 5' ends and varying points of 3'
termination is generated. The reaction mixture is then analyzed. The mass spectrometer is
15 sensitive enough to distinguish mass differences between successive fragments, allowing
sequence information to be generated.

Mass spectrometry sequencing is highly accurate, inexpensive, and rapid compared to
conventional methods. The major limitation, however, is that the read length is on the order
of tens of bases. Even the best method, matrix-assisted laser desorption ionization time-of-
20 flight (MALDI-TOF) mass spectroscopy (Smirnov et al., "Sequencing oligonucleotides by
exonuclease digestion and delayed extraction matrix-assisted laser desorption ionization time-
of-flight mass spectrometry," *Anal. Biochem.* 238:19-25, 1996), can only achieve maximum
read lengths of 80-90 base pairs. Much longer read lengths are physically impossible due to
fragmentation of longer DNA at guanidines during the analysis step. Mass spectrometry
25 sequencing is thus limited to verifying short primer sequences and has no practical application
in large-scale sequencing.

The Scanning tunneling microscope (STM) sequencing (Ferrell, "Scanning tunneling
microscopy in sequencing of DNA." In *Molecular Biology and Biotechnology*, R.A. Meyers,
Ed. VCH Publishers, New York, 1997) method was conceived at the time the STM was
30 commercially available. The initial promise of being able to read base-pair information
directly from the electron micrographs no longer holds true. DNA molecules must be placed
on conducting surfaces, which are usually highly ordered pyrolytic graphite (HOPG) or gold.
These lack the binding sites to hold DNA strongly enough to resist removal by the physical

and electronic forces exerted by the tunneling tip. With difficulty, DNA molecules can be electrostatically adhered to the surfaces. Even with successful immobilization of the DNA, it is difficult to distinguish base information because of the extremely high resolutions needed. With current technology, purines can be distinguished from pyrimidines, but the individual purines and pyrimidines cannot be identified. The ability to achieve this feat requires electron microscopy to be able to distinguish between aldehyde and amine groups on the purines and the presence or absence of methyl groups on the pyrimidines.

Enzymatic luminometric inorganic pyrophosphate detection assay (ELIDA) sequencing uses the detection of pyrophosphate release from DNA polymerization to determine the addition of successive bases. The pyrophosphate released by the DNA polymerization reaction is converted to ATP by ATP sulfurylase and the ATP production is monitored continuously by firefly luciferase. To determine base specificity, the method uses successive washes of ATP, CTP, GTP, and TTP. If a wash for ATP generates pyrophosphate, one or more adenines are incorporated. The number of incorporated bases is directly proportional to the amount of pyrophosphate generated. Enhancement of generated sequence information can be accomplished with parallel analysis of many ELIDA reactions simultaneously.

Exonuclease sequencing involves a fluorescently labeled, single-stranded DNA molecule which is suspended in a flowing stream and sequentially cleaved by an exonuclease. Individual fluorescent bases are then released and passed through a single molecule detection system. The temporal sequence of labeled nucleotide detection corresponds to the sequence of the DNA (Ambrose et al., "Application of single molecule detection to DNA sequencing and sizing," *Ber. Bunsenges. Phys. Chem.* 97:1535-1542, 1993; Davis et al., "Rapid DNA sequencing based on single-molecule detection," *Los Alamos Science*. 20:280-6, 1992; Jett et al., "High-speed DNA sequencing: an approach based upon fluorescence detection of single molecules," *J. Of Bio. Structure & Dynamics*. 7:301-9, 1989). Using a processive exonuclease, it theoretically is possible to sequence 10,000 bp or larger fragments at a rate of 10 bases per second.

In the sequencing by hybridization method, a target DNA is sequentially probed with a set of oligomers consisting of all the possible oligomer sequences. The sequence of the target DNA is generated with knowledge of the hybridization patterns between the oligomers and the target (Bains, "Hybridization methods for DNA sequencing," *Genomics*. 11:294-301, 1991; Cantor et al., "Reporting on the sequencing by hybridization workshop," *Genomics*.

13:1378-1383, 1992; Drmanac et al., "Sequencing by hybridization." In *Automated DNA Sequencing and Analysis Techniques*, J. Craig Ventor, Ed. Academic Press, London, 1994). There are two possible methods of probing target DNA. The "Probe Up" method includes immobilizing the target DNA on a substrate and probing successively with a set of oligomers. 5 "Probe Down" on the other hand requires that a set of oligomers be immobilized on a substrate and hybridized with the target DNA. With the advent of the "DNA chip," which applies microchip synthesis techniques to DNA probes, arrays of thousands of different DNA probes can be generated on a 1 cm² area, making Probe Down methods more practical. Probe Up methods would require, for an 8-mer, 65,536 successive probes and washings, which 10 would take an enormous amount of time. On the other hand, Probe Down hybridization generates data in a few seconds. With perfect hybridization, 65,536 octamer probes would determine a maximum of 170 bases. With 65,536 "mixed" 11-mers, 700 bases can be generated.

The most common limitation of most of these techniques is a short read length. In 15 practice a short read length means that additional genetic sequence information needs to be sequenced before the linear order of a target DNA can be deciphered. The short fragments have to be bridged together with additional overlapping fragments. Theoretically, with a 500 base read length, a minimum of 9×10^9 bases need to be sequenced before the linear sequence of all 3×10^9 bases of the human genome are properly ordered. In reality, the number of bases 20 needed to generate a believable genome is approximately 2×10^{10} bases. Comparisons of the different techniques show that only the impractical exonuclease sequencing has the theoretical capability of long read lengths. The other methods have short theoretical read lengths and even shorter realistic read lengths. To reduce the number of bases that need to be sequenced, it is clear that the read length must be improved.

25 Protein sequencing generally involves chemically induced sequential removal and identification of the terminal amino acid residue, e.g., by Edman degradation. See *Stryer, L., Biochemistry, W. H. Freeman and Co., San Francisco (1981) pp. 24-27*. Edman degradation requires that the polypeptide have a free amino group which is reacted with an isothiocyanate. The isothiocyanate is typically phenyl isothiocyanate. The adduct intramolecularly reacts with 30 the nearest backbone amide group of the polymer thereby forming a five membered ring. This adduct rearranges and the terminal amino acid residue is then cleaved using strong acid. The released phenylthiohydantoin (PTH) of the amino acid is identified and the shortened polymer can undergo repeated cycles of degradation and analysis.

Further, several new methods have been described for carboxy terminal sequencing of polypeptides. See Inglis, A. S., Anal. Biochem. 195:183-96 (1991). Carboxy terminal sequencing methods mimic Edman degradation but involve sequential degradation from the opposite end of the polymer. See Inglis, A. S., Anal. Biochem. 195:183-96 (1991). Like
5 Edman degradation, the carboxy-terminal sequencing methods involve chemically induced sequential removal and identification of the terminal amino acid residue.

More recently, polypeptide sequencing has been described by preparing a nested set (sequence defining set) of polymer fragments followed by mass analysis. See Chait, B. T. et al., Science 257:1885-94 (1992). Sequence is determined by comparing the relative mass
10 difference between fragments with the known masses of the amino acid residues. Though formation of a nested (sequence defining) set of polymer fragments is a requirement of DNA sequencing, this method differs substantially from the conventional protein sequencing method consisting of sequential removal and identification of each residue. Although this method has potential in practice it has encountered several problems and has not been
15 demonstrated to be an effective method.

Each of the known methods for sequencing polymers has drawbacks. For instance most of the methods are slow and labor intensive. The gel based DNA sequencing methods require approximately 1 to 3 days to identify the sequence of 300-800 units of a polymer. Methods such as mass spectroscopy and ELIDA sequencing can only be performed on very
20 short polymers.

A need exists for *de nouveau* polymer sequence determination. The rate of sequencing has limited the capability to generate multiple body and temporal expression maps which would undoubtedly aid the rapid determination of complex genetic function. A need also exists for improved systems and methods for analyzing polymers in order to speed up the rate
25 at which diagnosis of diseases and preparation of new medicines is carried out.

Summary of the Invention

The invention relates to new systems, methods and products for analyzing polymers and in particular new systems, methods and products useful for determining the sequence of
30 polymers. The invention has numerous advantages over prior art systems and methods used to sequence polymers. Using the methods of the invention the entire human genome could be sequenced several orders of magnitude faster than could be accomplished using conventional technology. In addition to sequencing the entire genome, the systems, methods and products

of the invention can be used to create comprehensive and multiple expression maps for developmental and disease processes. The ability to sequence an individual's genome and to generate multiple expression maps will greatly enhance the ability to determine the genetic basis of any phenotypic trait or disease process.

5 According to one aspect, a system for optically analyzing a polymer of linked units includes an optical source, an interaction station, an optical detector, and a processor. The optical source is constructed to emit radiation of a selected wavelength. The interaction station is constructed to receive the emitted radiation and produce a localized radiation spot from the radiation emitted from the optical source. The interaction station is also constructed
10 to sequentially receive units of the polymer and arranged to irradiate sequentially the units at the localized radiation spot. The optical detector is constructed to detect radiation including characteristic signals resulting from interaction of the localized radiation spot with the units. The processor is constructed and arranged to analyze the polymer based on the detected radiation.

15 Preferred embodiments of this aspect include one or more of the following features:

 The interaction station is constructed to sequentially receive the units being selectively labeled with a radiation sensitive label and the interaction includes interaction of the localized radiation with the radiation sensitive label.

 The radiation sensitive label includes a fluorophore.

20 The interaction station includes a waveguide constructed to receive the emitted radiation and provide the evanescent radiation in response thereto.

 The interaction station includes a slit having a width in the range of 1 nm to 500 nm, wherein the slit produces the localized radiation spot.

 The interaction station includes a microchannel and a slit having a submicron width
25 arranged to produce the localized radiation spot. The microchannel is constructed to receive and advance the polymer units through the localized radiation spot.

 The width of the slit is in the range of 10 nm to 100 nm.

 The system may include a polarizer and the optical source is a laser constructed to emit a beam of radiation and the polarizer is arranged to polarize the laser beam prior to reaching the
30 slit.

 The polarizer may be arranged to polarize the laser beam in parallel to the width of the slit, or perpendicular to the width of the slit.

 The interaction station may include several slits located perpendicular to the microchannel

that is arranged to receive the polymer in a straightened form.

The interaction station may include a set of electrodes constructed and arranged to provide electric field for advancing the units of the polymer through the microchannel.

The system may further include an alignment station constructed and arranged to
5 straighten the polymer and provide the straightened polymer to the interaction station.

In another embodiment a method for optically analyzing a polymer of linked units comprising:

- labeling selected units of the polymer with radiation sensitive labels;
- sequentially passing the units of the polymer through a microchannel;
- 10 generating radiation of a selected wavelength to produce therefrom a localized radiation spot;
- irradiating sequentially the labeled units of the polymer at the localized radiation spot;
- detecting sequentially radiation providing characteristic signals resulting from interaction of the localized radiation spot with the labels or the units; and
- 15 analyzing the polymer based on the detected radiation.

In another embodiment, an article of manufacture used for optically analyzing a polymer of linked units, comprising an interaction station fabricated on a substrate and constructed to receive radiation and produce therefrom a localized radiation spot. The interaction station is further constructed to sequentially receive units of the polymer and
20 arranged to irradiate sequentially the units at the localized radiation spot to generate characteristic signals of radiation.

According to another aspect, a system for optically analyzing a polymer of linked units includes an optical source, an interaction station, an optical detector, and a processor. The optical source is constructed to emit radiation of a selected wavelength. The interaction
25 station is constructed to receive the emitted radiation and constructed to sequentially receive units of the polymer and arranged to irradiate sequentially the units of the polymer with evanescent radiation excited by the radiation emitted from the source. The optical detector is constructed to detect radiation including characteristic signals resulting from interaction of the evanescent radiation with the units. The processor is constructed and arranged to
30 analyze the polymer based on the detected radiation.

Preferred embodiments of this aspect include one or more of the following features:

The interaction station is constructed to sequentially receive the units being selectively labeled with a radiation sensitive label and the interaction includes interaction of

localized radiation spot; and a processor constructed and arranged to analyze said polymer based on said detected radiation including said characteristic signals.

In one embodiment the interaction station is constructed to sequentially receive said units being selectively labeled with a radiation sensitive label producing said characteristic signals at said localized radiation spot. In another embodiment the radiation sensitive label includes a fluorophore. In some embodiments the filter is a laser line filter.

The system may also include an objective, wherein the objective focuses said filtered optical radiation.

The proposed system and method for analyzing polymers is particularly useful for determining the sequence of units within a DNA molecule and can eliminate the need for generating genomic libraries, cloning, and colony picking, all of which constitute lengthy pre-sequencing steps that are major limitations in current genomic-scale sequencing protocols. The methods disclosed herein provide much longer read lengths than achieved by the prior art and a million-fold faster sequence reading. The proposed read length is on the order of several hundred thousand nucleotides. This translates into significantly less need for overlapping and redundant sequences, lowering the real amount of DNA that needs to be sequenced before genome reconstruction is possible. The actual time taken to read a given number of units of a polymer is a million-fold more rapid than current methods because of the tremendous parallel amplification supplied by a novel apparatus also claimed herein, which is referred to as a nanochannel plate or a microchannel plate. The combination of all these factors translates into a method of polymer analysis including sequencing that will provide enormous advances in the field of molecular and cell biology.

Brief Description of the Drawings

Fig. 1 illustrates diagrammatically a system for characterizing polymers.

Fig. 2 illustrates an alignment and a first interaction station used in the system of Fig. 1.

Fig. 3 is a cross-sectional view of the alignment and the first interaction station along lines 3-3 shown in Fig. 2.

Fig. 4 is a top view of a portion of the alignment and the first interaction station shown in Fig. 2.

Fig. 4A illustrates the arrangement of a nanoslit located in the first interaction station shown in Fig 4.

Fig. 4B illustrates an optical system for characterizing polymer units labeled by a

fluorophore.

Figs. 5 and 5A illustrate a second interaction station used in the system of Fig. 1.

Figs. 6 through 7B illustrate the fabrication of the alignment and first interaction station shown in Fig 4.

5 Fig. 8 is an SEM micrograph of the fabricated alignment and first interaction stations.

Figs. 9, 10A, 10B, and 10C show results of a test measurement of the alignment and interaction station of Fig. 8.

Fig. 11 is a cross-sectional view of the central line of optical waveguides according to another embodiment of the first interaction station.

10 Fig. 11A is a perspective view of the optical waveguides shown in Fig. 11

Figs. 11B and 11C illustrate the interaction of with a linearized polymer with evanescent radiation emitted from the optical waveguide.

Fig. 12 illustrates optical systems for near-field and far-field detection as used with the optical waveguide of Fig. 11.

15 Figs. 13, 13A and 13B illustrate coupling of electromagnetic radiation into the optical waveguide of Fig. 11.

Figs. 14A through 16G illustrate the fabrication of the optical waveguides shown in Fig. 11.

20 Fig. 17 is a schematic of an optical apparatus which utilizes confocal fluorescence illumination and detection for linear analysis of polymers.

Fig. 18 is a top view of another embodiment of the alignment station for aligning and stretching polymer.

25 **Detailed Description of the Preferred Embodiments**

Referring to Fig. 1, an interactive system for characterizing individual units of a polymer includes a system controller 10, a polymer supply 20, a microfluidic pump 25, a polymer alignment station 30, a first interaction station 40, and a second interaction station 50. System controller 10 may be a general purpose computer. Microfluidic pump 25 supplies
30 selected amounts of polymer 27 from polymer supply 20 to polymer alignment station 30. Polymer alignment station 30, controlled by system controller 10, straightens and aligns individual polymers using force field and mechanical obstacles, and dispenses the polymers to first interaction station 40. The first interaction station 40 uses an optical system for

characterizing individual units of the polymer passing through. The optical system includes an optical source 42, an optical filter 45, an optical detector 46 and other optical elements and electronic elements associated with the source and detector. The optical system is controlled by an optical controller 48.

5 As the individual units the polymer pass through interaction station 40, optical source 42 emits radiation directed to an optical component of interaction station 40. The optical component produces a localized radiation spot that interacts directly with polymer units, or interacts with labels selectively attached to the polymer units, or interact with both the polymer units and the labels. The localized radiation spot includes non-radiating near field or
10 an evanescent wave, localized in at least one dimension. The localized radiation spot provides a much higher resolution than the diffraction-limited resolution used in conventional optics.

Furthermore, interaction station 40 uses unique arrangements and geometries that allow the localized radiation spot to interact with one or several polymer units or attached labels that are on the order of nanometers or smaller. Optical detector 46 detects light modified by the
15 interaction and provides a detection signal to optical controller 48. Second interaction station 50 uses electric or electromagnetic field, X-ray radiation, or visible or infrared radiation for characterizing the polymer passing from first interaction station 40 through second interaction station 50. A controller 56 controls the operation of second interaction station 50. Both
20 controllers 48 and 56 are connected to system controller 10.

Referring to Figs. 2 and 3, polymer alignment station 30 and first interaction station 40 include a substrate 92, a quartz wafer 60, and a glass cover 90, which is optional. Substrate 92 is machined from a non-conducting, chemically inert material, such as Teflon® or Delrin®, to facilitate a flow of conducting fluid 96 (for example, agarose gel) and the examined polymer. Substrate 92 includes trenches 94A and 94B machined to receive gold wires 98A and 98B,
25 respectively, which have a selected shape in accordance with the shape of the electric field used for advancing polymer molecules 39 across first interaction station 40. Quartz wafer 60 is sealed onto substrate 92 around regions 91.

Alternatively, trenches 94A and 94B and wires 98A and 98B may be replaced by metallic regions located directly on quartz wafer 60, or may be replaced by external electrodes for
30 creating the electric field. In general, the electrodes are spaced apart over a distance in the range of about millimeter to 5 centimeters, and preferably 2 centimeters and provide typically field strengths of about 20 V/cm.

Figs. 4 and 4A show a presently preferred embodiment of alignment station 30 and first

interaction station 40. Fig. 4 is a top view of a portion of alignment station 30A and first interaction station 40 (also shown in Fig. 2), which are fabricated on quartz wafer 60. Of course, a single quartz wafer 60 may include hundreds or thousands of the alignment and first interaction stations. Quartz wafer 60 includes a quartz substrate covered with a metal layer 62 (e.g., aluminum, gold, silver) and having a microchannel 41 fabricated on the surface.

Fabricated through metal layer 62 are slits 36A, 36B and 36C, which form the optical elements that provide the localized radiation spot. Slits 36A, 36B and 36C have a selected width in the range between 1 nm and 5000 nm, and preferably in the range between 10 nm and 1000 nm, and more preferably in the range between 10 nm and 100 nm. Slits 36A, 36B and 36C are located across microchannel 41, which has a width in the range of 1 micrometer to 50 micrometers and a length of several hundred micrometers. The electric field, created by gold wires 98A and 98B, pulls a polymer chain 39 (such as a DNA molecule) through microchannel 41 pass slits 36A, 36B and 36C.

As shown in Fig. 4, polymer alignment station 30 includes several alignment posts 32 located in regions 31. Regions 31 are connected via transition regions 34 to microchannel 41. Alignment posts 32 have a circular cross-section and are about 1 micron in diameter.

Alignment posts 32 are spaced about 1.5 microns apart and located about 5 μm to 500 μm (and preferably about 10 μm to 200 μm) from microchannel 41 depending on the length of the examined polymer. For example, when the polymer is bacteriophage T4 DNA, which has about 167 000 base pairs, alignment posts 32 are located about 30 μm from nanoslit 36A. In general, the distance from nanoslit 36A is about one half of the expected length of polymer 39.

Fig. 4A illustrates interaction of a light beam 65, emitted from optical source 42, with a nanoslit 36, formed in metal layer 62, to produce a localized radiation spot 67. Laser beam 65, which has a size many times larger than the width of nanoslit 36, irradiates the back side of quartz wafer 60, propagates through quartz wafer 60 and interacts with nanoslit 36, as shown by the E-field lines. Localized radiation spot 67, which is a non-radiating near field, irradiates sequentially the units of polymer chain 39 as polymer chain 39 is pulled through microchannel 41. Localized radiation spot 67 may be understood as an evanescent wave emitted from nanoslit 36. Because the width of nanoslit 36 is smaller than the wavelength of light beam 65 the radiation is in the Fresnel mode.

The optical system may also include a polarizer 43 placed between optical source 42 and quartz wafer 60, and a notch filter 45, placed between quartz wafer 60 and optical detector

46. When the polarizer orients light beam 65 with the E vector parallel to the length of nanoslit 36, there is near-field radiation emitted from nanoslit 36 and no far field radiation. When the polarizer orients light beam 65 with the E vector perpendicular to nanoslit 36 (which is many wavelengths long), there is far-field emission from nanoslit 36. By selectively polarizing the incident beam 65, the optical system can switch between the near-field and far-field emissions.

Fig. 4B illustrates an optical system for characterizing polymer units labeled by a fluorophore. The optical system includes a laser source 80, an acousto-optic tunable filter 82, a polarizer 84, a notch filter 86, an intensifier and a CCD detector 88, and a video monitor 90 connected to a video recorder VCR 92. The individual units of polymer chain 39 are selectively labeled by a fluorophore 68 sensitive to a selected excitation wavelength. Acousto-optic tunable filter 82 is used to select the excitation wavelength of light emitted from laser source 80. The excitation beam 65 interacts with nanoslit 36 (shown in Fig. 4A and designated here as region 40) to create the non-radiating near-field 67. The electric field between gold wires 98A and 98B (Figs. 2 and 3) pulls polymer chain 39 at a known rate causing interaction of each labeled unit with radiation 67. As fluorophore 68 moves pass slits 36A, 36B and 36C (shown Fig. 4), emitted radiation 67 excites fluorophore 68 that re-emits fluorescent radiation 72. Notch filter 86 passes the fluorescent wavelength (72) of radiation 70 and attenuates the excitation wavelength to increase the signal to noise resolution, as is known in the art. CCD detector 88 located few millimeters to few centimeters above quartz wafer 60 detects fluorescent radiation 72. CCD detector 88 can detect separately for each nanoslits 36A, 36B and 36C fluorescent radiation 72 as the fluorophore moves across. This process occurs at a large number of nanoslits located on quartz wafer 60.

Electric field may be used to position polymer 39 close to nanoslit 36. Nanoslit 36 "emits" the non-radiating field 67, which is attenuated over a distance of only one or two wavelengths. To position fluorophore 68 within the range of the non-radiating field 67, polymer 39 may need to be pulled closer to nanoslit 36 (and metal film 62) and thus closed to metal layer 62. Polymer 39 is pulled closer to nanoslit 36 using dielectric forces created by applying AC field to metal layer 62. See, e.g., "Trapping of DNA in Nonuniform Oscillating Electric Fields," by Charles L. Ashbury and Ger van den Engh, Biophysical Journal Vol 74, pp 1024-1030 (1998), "Molecular Dielectrophoresis of Biopolymers," by M. Washizu, S. Suzuki, O. Kurosawa, T. Nishizaka, and T. Shinohara, in IEEE Transactions on Industry Applications, Vol 30, No 4, pp. 835-843 (1994), and "Electrostatic Manipulation of DNA in

Microfabricated Structures," by M. Washizu, and O. Kurosawa, in IEEE Transactions on Industry Applications, Vol 26, No 6, pp. 1165-1172 (1990). In general, see "Dielectrophoresis: The Behavior of Neutral Matter in Nonuniform Electric Fields," by Pohl, H. A., Cambridge University Press, Cambridge, UK, 1978. The inhomogeneous field will attract polarized units of polymer 39 (e.g., DNA molecule) to metal layer 62.

Referring to Fig. 5 second interaction station 50 measures ionic current across a nanochannel as linearized polymer molecules approach the nanochannel and pass through. The detected blockages of the ionic current are used to characterize the length of the polymer molecules and other characteristics of the polymer. Interaction station 50 receives linearized polymer 39 from first interaction region 40 and applies transchannel voltage using electrodes 52 and 53 in a direction perpendicular to electrodes 54 and 55 to draw the polymer molecules through a channel 51. Electrodes 54 and 55 are connected to a microampere meter 56A, located in controller 56, to measure the ionic current across nanochannel 51. Alternatively, referring to Fig. 5A, the microampere meter is replaced by a bridge 56B, which compares the impedance of channel 51 without polymer 39 (Z_1) with the instantaneous impedance of (Z_x). Without polymer 39 present in channel 51, the voltmeter measures 0 V. As the extended, nearly linear string 39 passes through channel 51, its presence detectably reduces, or completely blocks, the normal ionic flow from electrode 54 to electrode 55.

Electrodes 54 and 55 are fabricated using submicron lithography and are connected to the bridge to detect changes in the impedance or the microampere meter to measure the ionic current. The measured data across the channel are amplified, and the amplified signal is filtered (e.g., 64,000 samples per second) using a low pass filter, and the data is digitized at a selected sampling rate by an analog-to-digital converter. System controller 10 correlates the transient decrease in the ionic current with the speed of the polymer units and determines the length of the polymer, for example the length of a DNA or RNA molecule.

In another embodiment, the optical system includes an ultra fast, highly sensitive spectrophotometer capable of detecting fluorescence from a single fluorophore. Optical source 42 is a mode-locked Nd:YAG laser emitting radiation of an excitation wavelength. The system uses a splitter providing a reference beam to a photodiode and a discriminator (e.g., Tennelec TC454) that provides the start pulse to a time-to-amplitude converter (e.g., Tennelec 863). The primary beam 65 is directed through a neutral density filter that adjusts the power level. As described above, fluorophore 68 interacting with non-radiation near-field 67 excites fluorescent light 72, which is collected by detector 46 after being spectrally filtered by an

interference filter (e.g., made by Omega Optics) and detected by an avalanche photodiode or a photomultiplier (e.g., Hamamatsu R1562UMCP microchannel photomultiplier). The microchannel photomultiplier signal is amplified by an amplifier and shaped by a discriminator (for example, Tennelec C4534 discriminator). The signal having appropriate time delays are provided to the time-to-amplitude converter (TAC). The time-gated TAC output is counted by a multiscaler and interfaced via a VME interface to system controller 10. System controller 10 provides, for signal from each detector, a time-delay histogram that is characteristic for each type of the fluorescing fluorophore coupled to a unit of polymer 39.

Different fluorophores have different fluorescent lifetimes (i.e., the average amount of time that the molecule remains excited before returning to the ground electronic state through the emission of a fluorescent photon) that usually have an exponential probability distribution. Fluorescent lifetime is useful for identification of the fluorophore. In rapid sequencing, the system can use related dyes with similar spectra but different lifetimes thus employing only one laser source emitting the excitation wavelength and one detector detecting the fluorescent radiation.

In another embodiment, the optical system uses modulated radiation (e.g., single side band or double side band modulation) at frequencies in the range of 10 MHz to 1 GHz using phase modulation techniques to characterize fluorescence of a single fluorophore located next to a polymer unit. For example, a laser source emits a light beam 65, which is intensity modulated using a sinusoidal signal at a frequency of 100 MHz. The excited fluorescent radiation 72 is detected using a photomultiplier. The corresponding signal is homodyne or heterodyne detected to resolve the characteristic signal from the fluorophore, e.g., fluorescent lifetime. (See, for example, Lackowicz, J.R., "Gigahertz Frequency-Domain Fluorometry: Resolution of Complex Intensity Decays, Picosecond Processes and Future Developments," Photon Migration in Tissues, Academic Press, NY, pp.169-186, 1989; see also other references cited therein)

Figs. 6 through 7B illustrate the fabrication of alignment region 30, microchannel 41 and slits 36A, 36B and 36C, shown in Fig. 4. Fig. 6 is a side view of quartz wafer 60, which is about 400 microns thick and polished on both sides. First a 300 nm thick aluminum film 62 is evaporated on the wafer and primed in hexamethyldisiloxane (HMDS) for 35 minutes (Fig. 6). Then, a photoresist Shipley 1813 was spun onto the wafers at 4000 rpm 60 sec., and the wafer was baked on a hotplate at 115°C to harden the resist (Fig. 6A). The wafer was exposed, and the photoresist developed in 1:1 MF 312 developer and water for 60 seconds.

The coarse aluminum pattern was etched using a Cl reactive ion etcher PK 1250 for 1.5 min. (Fig. 6B). Fig. 6C shows an overview of the wafer with the devices shown as squares and alignment marks as crosses. All resist residues were removed using the resist descum process in the Branson barrel etcher at 1000 W RF power for 10 minutes (Fig. 6D).

5 Referring to Fig. 6E, the PMMA resist (4% 950 K in MIBK) was spun onto the wafers at 3000 rpm for 60 seconds and the wafer was baked on a hotplate at 180°C for 30 min. Then a 100 Å layer of gold metal was evaporated onto the PMMA photoresist to avoid a charge build-up. The PMMA photoresist was exposed in a e-beam system to define the nanoslits. The exposed PMMA resist was developed in IPA:MIBK 3:1 for 1min., and the 100 Å layer of gold
10 was metal was etched (Fig. 6F). Next, the nanoslit patterns were defined by etching aluminum using the Cl reactive ion etch PK 1250 for 1.5 min (Fig. 6G). The photoresist was removed using the Branson barrel etcher at 1000 W RF power for 10 minutes (Fig. 6H). To create alignment region 30 and microchannel 41, a one micron layer of SiO₂ was deposited using plasma enhanced chemical vapor deposition (PECVD) at T=240 C, 450 mTorr, 50 W
15 RF power using 15 sccm silane, 50 sccm N₂O (Fig. 6I). The SiO₂ layer was planarized by chemical mechanical polishing (CMP).

Figs. 7 through 7B are side views of the wafer along one of the nanochannels. Referring to Fig. 7, alignment region 30 and microchannel 41 were defined by first spinning photoresist Shipley 1813 onto the wafers at 1800 rpm for 60 sec. and baking the resist on a
20 hotplate at 115°C for 60 sec. The resist was exposed in a high resolution mask aligner, such as a 5x g-line stepper, and developed in 1:1 MF 312 and water for 60 sec. The SiO₂ layer was etched (Fig. 7A) using reactive ion etching (RIE) in CHF₃ (50 sccm) + O₂ (2 sccm) to define the pattern in the SiO₂ layer as shown in Fig. 4. The photoresist was removed using the Branson barrel etcher at 1000 W RF power for 10 minutes. Next, a protective SiO₂ layer of
25 10 nm to 100 nm was deposited deposited PECVD (Fig. 7B). Glass cover 90 (shown in Fig. 2) may be anodically bonded to quartz wafer 60, or may be attached to chip 60 using a thin layer of RTV.

Fig. 8 shows an SEM micrograph with two fabricated alignment regions 30 and two interaction regions 40. Each alignment region 30 includes microposts 31, and each interaction
30 regions 40 includes microchannel 41 and nanoslits 36A, 36B, and 36C, as drawn in Fig. 4.

Referring to Figs. 9 through 10C, the fabricated alignment regions 30 and interaction regions 40 (shown in Fig. 8) were tested in the following experiment.

CW laser light from a collimated Ar:Kr ion laser was focused onto the back side of wafer 60

as shown in Fig. 4A. Laser beam 65, having excitation wavelength of 488 nm, created a non-radiating near field on the other side film 62 near a fluorophore 68. A microscope objective captured the fluorescent far-field radiation of 560 nm, which was recorded in a time-dependent manner by a photomultiplier. This time-dependent signal then gave a record of the pas-sage of the object over the slit with a spatial resolution roughly equal to the width of the slit 36.

Fig. 9 shows a response of the photomultiplier for 0.5 micron balls passing a 2.0 micron wide slit (curve 94A) and 0.1 micron wide slit (curve 94B). Curves 94A and 94B represent the voltage of the photomultiplier as a function of time. As expected, the smaller slit produces the narrower curve 94B, which is the minimum response of this setup.

Figs. 10A through 10C show the imposition of fluorescent beads and yoyo-1 stained T4 DNA simultaneously passing through two nanoslits which are spaced 10 μ m apart. In Fig. 10A, two intensity peaks bead passing through the first slit and then through the second slit. Fig. 10B shows a partly uncoiled strand of DNA passing through the delivery channel. Broader Peaks 96A and 96B are due to the Geometry of the DNA coil. The passage of the fluorescent bead is superimposed of the DNA signal. Fig. 10C shows a highly extended DNA in transit through three slits, 36A, 36B and 36C. Again, for reference, the signal from a fluorescent bead is superimposed on the DNA signal. Broader peaks 97A, 97B and 97C are due to the geometry of the DNA coil.

Fig. 11 is a cross-sectional view of quartz wafer 150 with waveguide 160 taken along a central axis of the waveguide. Waveguide 160 includes and two waveguides 166A and 166B with a rectangular cross-section fabricated on quartz wafer 150. Rectangular waveguides 166A and 166B may be rectangular dielectric waveguides that use two dielectric materials with different refractive indexes and confine light in a core material with a larger refractive index (n_2) than the refractive index (n_1) of the surrounding dielectric material ($n_2 > n_1$). Alternatively, rectangular waveguides 166A and 166B may be rectangular mirror waveguides that use a dielectric core material surrounded by a metallic material, or waveguides 166A and 166B by be formed by a combination of the two types of waveguides.

The rectangular dielectric waveguides ideally achieve the total internal reflection of light propagation, where the incident angle $\theta_i > \theta_c$. To confine the introduced light using total internal reflection, interaction station 40 uses a triangular waveguide with a very small angle at the tip. Rectangular mirror waveguides usually exhibit a higher loss depending on the quality of the metallic mirrors. Rectangular mirror waveguides convey light up to a

wavelength (λ) equal twice the height (h) of the waveguide ($\lambda = 2 \cdot h$). Thus these waveguides have a height designed for propagation of light in a selected range of wavelengths useful for polymer examination. For further details see "Fundamentals of Photonics," by Bahaa E. A. Saleh and Malvin Carl Teich, John Wiley & Sons, 1991.

5 As shown in a perspective view in Fig. 11A, waveguides 166A and 166B are located symmetrically with their tips 170A and 170B aligned along the symmetry axis defining a nanochannel 171 (shown in Fig. 11B). Nanochannel 171 has a width in the range of 2 nm to 100 nm, and preferably in the range of 5 nm to 50 nm. Gold wires 198A and 198B (shown in Figs. 2 and 3) are spaced about 3 to 25 millimeters from nanochannel 171. Alternatively, as
10 shown in Fig. 11C, the two waveguide arrangement may be replaced by a single waveguide with an opposite electrode forming a wider channel in the range of 100 nm to 1 μ m.

Triangular waveguides 166A and 166B shown in Figs. 11 and 11A are about 10 μ m wide, 5000 μ m long, and over 1 μ m high and are made of SiO_2 . Waveguides 166A and 166B are isolated from substrate 162 by a metallic layers 164A and 164B and from a glass cover
15 152 by metallic layers 174A and 174B, respectively. (Alternatively, metallic layers 164A and 174A for waveguide 166A, or metallic layers 164B and 174B waveguide 166B, may be replaced by dielectric layers with a lower refractive index.) The introduced plane wave 176 is coupled into triangular waveguide 166A at an input side 168A and undergoes internal reflection at waveguide sides 172A and 173A as it is transmitted toward waveguide tip 170A.
20 Waveguide tip 170A emits waves of evanescent radiation (illustrated in Fig. 11B) into nanochannel 171. In nanochannel 171, the evanescent radiation interacts with individual units of polymer 39 producing radiation with a characteristic signal. For example, the evanescent radiation interacts with a fluorophore located next to a specific unit of polymer 39. Triangular waveguide 166B collects the radiation including the characteristic signal (e.g., fluorescent
25 radiation) from nanochannel 171 and transmits this radiation toward coupling region 168B. As the collected radiation propagates inside waveguide 166B, the radiation may undergo the total internal reflection at the triangular sides 173A and 173B. The output side 168B, providing radiation 188, is optically coupled to optical detector 46 (Fig. 1). Furthermore, the radiation from nanochannel 171 is also emitted in the direction 189, through glass cover 152.
30 Another, external optical detector, located few millimeters to few centimeters above nanochannel 171 detects far-field radiation 189, as shown in Fig. 12.

Fig. 11B is a cross-sectional view of two triangular waveguides 166A and 166B surrounded by metal layers on each side, wherein the cross-hatched pattern denotes a metal

layer on waveguide sides 172A, 172B, 173A, and 173B. However, the metal layer does not cover completely the apex of tips 170A and 170B of triangular waveguides 166A and 166B. The metal layer at tips 170A and 170B may be removed during the etching or milling process that is used to create nanochannel 171, as described below. Waveguide 166A conveys introduced light beam 176 to tip 170A by confining substantially the entire wave inside the SiO₂ volume. At tip 170A, waveguide 166A emits evanescent waves 177, which are attenuated as q^{-1} wherein $q = n_{1,2} \omega/c [(\sin\theta_1/\sin\theta_c)^2 - 1]^{1/2}$ in a dielectric waveguide (see, e.g., "Optical Waves in Layered Media" by P. Yeh, John Wiley & Sons, 1988). Thus the evanescent wave is attenuated over a distance of only one or two wavelengths for the total internal reflection ($\theta_1 > \theta_c$). Waves of evanescent radiation 177 interact with the units of polymer 39 passing through nanochannel 171. For example, evanescent waves 177 interact with a fluorophore 178 selectively attached to a selected unit of polymer 39. Fluorophore 178 emits fluorescent radiation 179 propagating in all directions. Fluorescent radiation 179 is collected by waveguide 166B and conveyed to detector 46 (Fig. 1).

Fig. 11C is a cross-sectional view of another embodiment using a single triangular waveguide 166 and a metal electrode 185. A channel 171A formed between waveguide 166 and metal electrode 185 about 0.5 μm , which is significantly larger than nanochannel 171. Triangular waveguide 166 is surrounded by metal layers on all sides and is fabricated similarly as waveguides 166A and 166B (Fig. 4A), wherein the cross-hatched pattern denotes a metal layer on waveguide sides 172 and 173. Similarly as for waveguide 166A, tip 170 emits evanescent waves 177, which are attenuated over a distance of only one or two wavelengths. Therefore, polymer 39 has to be pulled closer to tip 170 than electrode 185 to irradiate fluorophore 178 with evanescent waves 177.

Polymer 39 is pulled closer to tip 170 using dielectric forces created by applying AC field to electrode 185 and waveguide 166, i.e., metal layers 164 and 174, in addition to the DC field applied across wires 98A and 98B. The AC field applied capacitively with respect to the DC field generates inhomogeneous field in nanochannel 171 as described above in connection with Fig. 4A.

Fig. 12 illustrates an optical system 100 for detecting near field and far field radiation emitted from nanochannel 171. Optical source 44 emits light beam 76, which is focused onto input side 168A of waveguide 166A using techniques described in connection with Figs 13 through 189B. After the interaction of evanescent waves 176 with polymer 39, the near field radiation is collected by waveguide 166B and optically coupled to optical detector 46 from

output side 168B. The far field 101, emitted in direction 89, is collected by a lens 102, filtered by a tunable filter 104 and provided to a PMT detector 106. Optical source 44, such as an LED or a laser diode may be incorporated onto quartz wafer 150. This arrangement would eliminate the need for an external optical source which as to be aligned with in put side 168A. The optical sources are made using a direct bandgap material, for example GaN for generating UV radiation, or GaP:N for generating radiation of a green wavelength.

Quartz wafer 150 may also include an integrated optical detector 46 in order to avoid external setup for detection and filtering. An integrated avalanche photodiode or a PIN photodiode, together with an insitu filter for filtering out the excitation wavelength, receive light beam 188. Various integrated optical elements are described in "Integrated Optoelectronics - Waveguide Optics, Photonics, Semiconductors," by Karl Joachim Ebeling, Springer-Verlag, 1992. For example, a corrugated waveguide is used as a contradirectional coupler so that light within a narrow frequency band will be reflected back resulting in a filtering action. Another filter is made using two waveguides with different dispersion relations in close proximity. Light from one waveguide will be coupled into the other for wavelengths for which there is a match in the index of refraction. By applying a voltage to the waveguides, the dispersion curve is shifted and the spectrum of the resulting filter is altered providing a tunable filter.

In another embodiment, optical system 110 is an ultra fast, highly sensitive spectrophotometer capable of detecting fluorescence from a single fluorophore as described above.

In another embodiment, optical system 120 uses radiation modulated at frequencies in the range of 10MHz to 1GHz as described above

Figs. 13 through 13B show different types of coupling of light from an external optical source into a waveguide. Referring to Fig. 13, lights source 42 emits light beam 176, which is focused onto the input side 168A of triangular waveguide 166A using a focusing lens 180. Alternatively, referring to Fig. 13A, a prism 182 is used to couple light beam 176 into triangular waveguide 166A. Light beam 176 is diffracted by prism 182 and undergoes inside the total internal reflection. Prism 182 is located on the surface of SiO₂ volume 166A and is arranged to optically couple beam 176 across a layer 184 into waveguide 66A. Referring to Fig. 13B, alternatively, a diffraction grating 186 is used to couple light beam 176 into triangular waveguide 166A. Grating 86 is fabricated on waveguide 166A so that it diffracts light beam 176 toward tip 170A. Alternatively, an optical fiber couples light beam 176 to

triangular waveguide 166A. Different ways to couple light into a waveguide are described in Fundamentals of Optics, by Clifford R. Pollock, Richard D. Irwin, Inc., 1995.

Waveguides 166A and 166B are fabricated on quartz or another insulating material to
5 avoid electrical currents in substrate 152. To achieve the required high definition in the
nanochannel region (i.e., 10 nm resolution), the fabrication process uses UV lithography alone
or in combination with deep UV lithography, e-beam lithography or X-ray lithography. The
contiguous waveguide is first defined using standard UV lithography, and then nanochannel
(or microchannel 171A described in connection with Fig. 11C) is defined in separate e-beam
10 or X-ray lithography steps. In waveguide embodiments that include a radiation slit at tips
170A and 170B, the slit (or a hole) is fabricated by creating a concave shape of the photoresist
(i.e., an undercut) at the very tips 170A and 170B of waveguides 166A and 166B, and by
creating a convex shape of the photoresist at the sides 172A, 173A, 172B and 173B before
evaporating the metal. Thus, the convex sides will be covered by the evaporated metal, but
15 not the concave tip. Alternatively, the small tip (the small hole) is fabricated by first creating
a very thin wall and then using lift-off or etching to create a metal film with the small slit over
the wall. When using e-beam lithography, metal hard masks are used to keep the resist
thickness down and the resolution high, as is known in the art.

Referring to Figs. 14A through 14K that are side views along the central line of
20 waveguides 166A and 166B are fabricated as follows: To improve adhesion of the resist to the
wafers, the wafers are primed in hexamethyldisiloxane (HMDS) for 34 minutes (Fig. 14A).
Then, a photoresist Shipley 1830 is spun onto the wafers at 4000 rpm 60 sec to achieve a 1.3
micron thick resist and the wafers are baked on a hotplate at 115 C for 60 sec to harden the
resist (Fig. 14B). The photoresist is exposed in a high resolution mask aligner such as a 5x
25 g-line stepper and baked in a pressurized NH_3 oven. This reverses the positive tone of the
photoresist and provides the necessary backward leaning profile (i.e., the undercut shown in
Fig. 14C) for the subsequent lift-off process. The wafer is flood exposed for 1 min in the
HTG/contact aligner with 405 nm light and developed with Microposit 321 for 1min.
Referring to Fig. 14D, a 1000 Angstrom Al layer is deposited and the lift-off is performed
30 using Microposit 1165 resist remover or acetone at room temperature (Fig. 14E). All resist
residues are removed using the resist descum process in the Branson Barrel etcher, 0.6 Torr O_2
at 150 W RF power.

Referring to Fig. 14F through 14K, the SiO_2 waveguide is created as follows: A 1

micron SiO_2 is deposited using plasma enhanced chemical vapor deposition (PECVD) at $T=240^\circ\text{C}$, 450 mTorr, 50 W RF power using 15 sccm silane, 50 sccm N_2O . The SiO_2 layer is planarized by chemical mechanical polishing (CMP), as shown in Fig. 14G. The top metal mask is defined by spinig photoresist Shipley 1830 onto the wafers at 4000 rpm for 60 sec to achieve a 1.3 micron thick resist and baking it on a hotplate at 115°C for 60 sec. The resist is exposed in a high resolution mask aligner, such as a 5x g-line stepper, and baked in a pressurized NH_3 oven. This reverses the positive tone of the photoresist and provides the necessary backward leaning profile (i.e., the undercut) for the subsequent lift-off process, as shown in Fig. 14I. The resist is flood exposed for 1 min in the HTG/contact aligner by 405 nm light and developed in Microposit 321 for 1min. As shown in Fig. 14J, a layer of 1000 Å Al metal is deposited. The excess metal is removed by a lift-off using the Microposit 1165 resist remover or acetone at room temperature.

Figs. 15A through 15G are side views along the central line and Figs. 16A through 16G are side views along a line perpendicular to the central line. The PMMA resist 496K is spun onto the wafers at 2500 rpm to achieve a 200 nm thick resist and bakes on a hotplate at 180°C for 60 min. to harden the resist. The PMMA is exposed by the e-beam system to create the pattern in the nanochannel region. The exposed PMMA resist is developed in IPA:MIBK 3:1 for 1min and a 1000 Å layer of Al metal is deposited as shown in Fig. 15C. After performing the lift-off of the excess metal in acetone, the waveguide is etched, but without the microchannel pattern, in the Plasma Therm 72 etcher using reactive ion etching (RIE) in CHF_3 (50 sccm) + O_2 (2 sccm) at 200 W RF power and 40 mTorr, > 1 micron to create a wall shown in Fig. 10B. The bottom metal is wet etched in the solution of 16 : H_2PO_4 ; 1 : HNO_3 ; 1 : acetic acid; 2 : water; wetting agent, or dry etched in Cl. The remaining resist is removed in a Branson Barrel O_2 plasma etcher at 1000 W RF power for 15 min. The aluminum is removed in a wet etch using 16 : H_2PO_4 ; 1 : HNO_3 ; 1 : acetic acid; 2 : water; wetting agent.

The deposition of the top Al layer over the waveguide is shown in Figs. 15E through 15G and 16D through 16G. Referring to Figs. 15 and 16D, a photoresist Shipley 1830 is spun onto the wafers at 4000 rpm for 60 sec to achieve a 1.3 micron thick resist and baked on a hotplate at 115°C for 60 sec. to harden the resist. The resist is exposed in a high resolution mask aligner, such as a 5x g-line stepper, and baked in a pressurized NH_3 oven. This reverses the positive tone of the photoresist and provides the necessary backward leaning profile (i.e., the undercut) for the subsequent lift-off process. The resist is flood exposed for 1 min in the

HTG/contact aligner 405 nm light and developed in Microposit 321 for 1min. A 1000 Å Al layer is deposited as shown in Figs. 15F and 16F. The excess metal is lifted-off using the Microposit 1165 resist remover or acetone at room temperature.

5 A layer of Cr metal is deposited on the top of the device as follows. First, a mask for the nanochannel was etched and then the Shipley 1830 resist was spun onto the wafers at 4000 rpm for 60 sec to achieve a 1.3 micron thick resist and baked on a hotplate at 115° C for 60 sec to harden the resist. The resist was exposed in a high resolution mask aligner, such as a 5x g-line stepper, and baked in a pressurized NH₃ oven. This process reverses the positive tone of the photoresist and provides the necessary backward leaning profile (i.e., the undercut) for
10 the subsequent lift-off process. The resist was flood exposed for 1 min in the HTG/contact aligner using 405 nm light and developed in Microposit 321 for 1min. Then, a 1000 Å Cr layer was deposited and a lift-off of excess metal was performed in the Microposit 1165 resist remover or acetone at room temperature. A PMMA 496K resist was spun onto the wafers at 2500 rpm to achieve a 200 nm thick resist and baked on a hotplate at 180° C for 60 min. to
15 harden the resist. The resist was exposed in the e-beam system to define the desired pattern, and the wafer was developed in IPA:MIBK 3:1 for 1min. Then, a 1000 Å Cr layer was deposited and the lift-off of excess metal was performed in the Microposit 1165 resist remover or acetone at room temperature.

Nanochannel 171 was crated by etching the first metal layer (i.e., the Al layer) in a Cl
20 based dry etch, wherein Cr acts as an etch mask. Then, the SiO₂ was etched in Plasma Therm 72 using reactive ion etching (RIE) in CHF₃ (50 sccm) + O₂ (2 sccm) at 200 W RF power and 40 mTorr, > 1 micron to create a wall. The bottom metal layer was etched in a Cl based dry etch and the remaining Cr was removed using a wet etch. Alternatively, nanochannel 171 can be fabricated by focussed ion beam milling to define the gap and the aperture in the tip.

25 For DNA sequencing, the individual molecules can be selectively labeled as described in the PCT application PCT/US98/03024 filed on Feb. 11, 1998, which is incorporated by reference. The sequencing is done using a combination of single-stranded DNA molecules (ssDNA), which have been hybridized with fluorescently tagged oligonucleotides of test sequences. When hybridization occurs, the tagged sequence is now at a fixed position on the
30 DNA molecule. The process can use three tags: "start" and "stop" tags, which signal the 3' and 5' beginning and end of the ssDNA, and the tagged oligo which is used for sequencing. By observing a large population of these tagged molecules using a spectrum of oligonucleotide sequences as they pass through the microchannel and recording the position

of the oligonucleotide labels, the system obtains the sequence of the molecule at an unprecedented level of speed, accuracy and low molecule concentration.

Another embodiment of the present invention is shown in Figure 17. An optical apparatus 200 utilizes confocal fluorescence illumination and detection. Confocal illumination allows a small optical volume (on the order of picoliters) to be illuminated. Both Raleigh and Raman scattering are minimized using a small probe volume. Optical apparatus 200 includes a light source 202, a filter 204, a dichroic mirror 206, an objective 208, a narrow band pass filter 210, a pinhole 212, a lens 214, and a detector 216. Light source 202, which is a 1 mW argon ion laser, emits a laser beam 201, which passes through filter 204. Filter 204 is a laser line filter that provides a focused beam of a wavelength of about 514 nm. The filtered beam 205 is reflected by dichroic mirror 206 and is focussed by objective 208 onto a region of a DNA sample or another polymer. Objective 208 is a 100x 1.2 NA oil immersion objective.

The DNA sample is a straightened DNA molecule with one or several units tagged by a fluorescent tag. The fluorescent tag on the DNA can be one of several dyes including Cy-3, tetramethylrhodamine, rhodamine 6G, and Alexa 546. In addition, intercalator dyes can be used such as TOTO-3 (Molecular Probes).

The excited tag provides a fluorescence emission that is passed through dichroic mirror 206, narrow bandpass filter 210 (e.g., manufactured by Omega Optical) and is focused onto a 100 μ m pinhole 212. The fluorescent light 213 is focussed by aspheric lens 214 onto detector 216, which is an avalanche photodiode (e.g., manufactured by EG&G Canada) operating in the photon counting mode. The output signal from the photodiode is collected by a multichannel scalar (EG&G) and analyzed using a general purpose computer.

The confocal apparatus is appropriate for quantitative applications involving time-of-flight. Such applications include measuring distances on the DNA, detecting tagged sequences, and determining degrees of stretching in the DNA. Single fluorescent molecules can be detected using the apparatus. Alternatively, an imaging apparatus uses an intensified CCD (ICCD, Princeton Instruments) mounted on a microscope.

Fig. 18 shows a presently preferred embodiment of alignment station 220 for aligning and stretching a polymers before they reach an interaction station 230, where they interact with optical radiation. Alignment station 220 is fabricated on a quartz wafer, which may be covered with a metal layer 222 (e.g, aluminum, gold, silver) Alignment station 220 includes a triangular microchannel 224, micropost region 228, and an entrance region 230, all fabricated on the surface.

Entrance region 230 is about 50 micron wide and is in communication with micropost region 228. Micropost region 228 includes several alignment posts 226. Alignment posts 226 have a circular cross-section and are about 1 micron in diameter. Alignment microposts 226 are spaced about 1.5 microns apart in 12 to 15 rows. Micropost region 228 is canted at about 26.6 degrees.

Microposts 226 are located about 100 μm to 5,000 μm (and preferably about 1,000 μm to 3,000 μm) from the interaction station, where the units of the polymer (e.g. DNA) interact with optical radiation. Microchannel 224 is a region of constant x-direction shear that maintains the polymer in extended conformation after release from microposts 226. The electric field pulls the examined polymer through microchannel 224.

A very effective technique of stretching a polymer (e.g., DNA) uniformly is to have an obstacle field inside the tapered microchannel 224, followed by a constant-shear section to maintain the stretching obtained and straighten out any remaining coiling in the polymer. The preferred embodiment is a structure that combines microposts with two regions of different funnel designs as shown in Fig. 18. Pressure flow is the preferred driving force because of the predictable behavior of fluid bulk flow.

A constant shear rate, or change in average velocity with distance in the channel, is defined as S:

$$u/x = S$$

where x is the distance down a substantially rectangular channel, and u is the average fluid velocity, which is computed from the overall fluid flow (Q) and the cross-sectional area (A) of the channel as follows:

$$u=Q/A$$

In one embodiment where the channel cross-section is rectangular, the channel may be defined by a constant height, H and width, W such that the cross-sectional area $A=HW$, and the average fluid velocity is given by:

$$u=Q/HW$$

Applying the boundary condition that the fluid flow must be continuous, Q is constant. Hence, u is inversely proportional to W. This relationship can be substituted into the original expression for S to determine a relationship between the shear rate and the width:

5
$$S = u/x = Q/H / x (1/W) = (-Q/HW^2) (dW/dx)$$

$$dW/dx = (-SH/Q)(W^2)$$

Integrating this expression, it is found that:

10

$$W = (SHx/Q + C)^{-1}$$

where C is a constant of integration determined by the original width of the channel (boundary condition). This equation for the width of the channel is used to define a channel beyond a post structure.

15

Other embodiments are within the following claims:

1. A system for optically analyzing a polymer of linked units comprising:
an optical source constructed to emit optical radiation of a known wavelength;
an interaction station constructed to receive said optical radiation and produce a localized
radiation spot from said optical radiation, said interaction station being also constructed to
sequentially receive units of said polymer and arranged to irradiate sequentially said units at
said localized radiation spot;
an optical detector constructed to detect radiation including characteristic signals resulting
from interaction of said units at said localized radiation spot; and
a processor constructed and arranged to analyze said polymer based on said detected
radiation including said characteristic signals.
2. The system of claim 1 wherein said interaction station is constructed to sequentially
receive said units being selectively labeled with a radiation sensitive label producing said
characteristic signals at said localized radiation spot.
3. The system of claim 2 wherein said radiation sensitive label includes a fluorophore.
4. The system of claim 1 wherein said interaction station includes a slit having a width in
the range of 1 nm to 500 nm, said slit producing said localized radiation spot.
5. The system of claim 1 wherein said interaction station includes a microchannel and a
slit having a submicron width arranged to produce said localized radiation spot, said
microchannel being constructed to receive and advance said polymer units through said
localized radiation spot.
6. The system of claim 1 wherein said width is in the range of 10 nm to 100 nm.
7. The system of claim 5 further including a polarizer and wherein said optical source
includes a laser constructed to emit a beam of said radiation, said polarizer being arranged to
polarize said beam prior to reaching said slit.
8. The system of claim 5 wherein said polarizer is arranged to polarize said beam in
parallel to said width of said slit.

9. The system of claim 5 wherein said polarizer is arranged to polarize said beam perpendicular to said width of said slit.

10. The system of claim 5 wherein said interaction station includes several said slits
5 intersecting said microchannel being arranged to receive said polymer in a straightened form.

11. The system of claim 5 further including a set of electrodes constructed and arranged to provide electric field for advancing said units of said polymer through said microchannel.

10 12. The system of claim 11 wherein said electrodes are internal electrodes.

13. The system of claim 11 wherein said electrodes are external electrodes.

14. The system of claim 5 wherein said nanoslit is several micrometers long.

15 15. The system of claim 5 further including an alignment station constructed and arranged to straighten said polymer and provide said straightened polymer to said microchannel, said alignment station including several microposts of about 1 μm in diameter and being spaced about 0.5 μm to 5 μm apart.

20 16. The system of claim 5 further including an alignment station constructed and arranged to straighten said polymer and provide said straightened polymer to said microchannel, said alignment station including several microposts being located at a distance of about 5 μm to 500 μm from said slit.

25 17. The system of claim 16 wherein said microposts are spaced 0.5 μm to 2.5 μm apart.

18. The system of claim 1 wherein said optical source is a laser and said system further including an acousto-optic tunable filter arranged to select said wavelength.

30 19. The system of claim 18 wherein said wavelength is an excitation wavelength of a fluorophore selectively coupled to said units and said characteristic signal being a fluorescent wavelength emitted by said fluorophore.

20. The system of claim 19 further including a notch filter arranged to transmit only said fluorescent wavelength to said optical detector.

21. The system of claim 1 wherein said optical source is constructed to emit said
5 wavelength in the range of ultraviolet to infrared wavelengths.

22. The system of claim 1 wherein said optical detector includes one of the following: a photodiode, an avalanche photodiode, a photomultiplier, a PIN diode, and a CCD.

10 23. The system of claim 1 wherein said processor is arranged to evaluate said characteristic signal being a fluorescent lifetime.

24. The system of claim 1 wherein said processor is arranged to evaluate said
15 characteristic signal being a fluorescent wavelength.

25. The system of claim 1 wherein said processor is arranged to evaluate said
characteristic signal being intensity of said detected optical radiation.

20 26. The system of claim 1 wherein said processor is arranged to evaluate said characteristic signal being a time dependent property of said detected optical radiation.

27. A method for optically analyzing a polymer of linked units comprising:
sequentially passing said units of said polymer through a microchannel;
generating optical radiation of a known wavelength to produce a localized radiation spot;
25 irradiating sequentially said units of said polymer at said localized radiation spot;
detecting sequentially radiation providing characteristic signals resulting from interaction
of said units at said localized radiation spot; and
analyzing said polymer based on said detected radiation including said characteristic
signals.

30 28. The method of claim 27 wherein said passing said polymer through said microchannel includes employing electric field.

29. The method of claim 27 wherein said producing said localized radiation spot includes optically coupling said generated light to a nanoslit having a width less than one μm .

30. The method of claim 27 wherein said producing said localized radiation spot includes optically coupling said generated light to a nanoslit having a width in the range of about 1 nm to 500 nm.

31. The method of claim 27 wherein said producing said localized radiation spot includes optically coupling said generated light to several nanoslits having their length oriented perpendicularly to said microchannel.

32. The method of claim 29 wherein said producing said localized radiation spot includes generating said light in form of a laser beam and polarizing said laser beam to be oriented in parallel to said width of said slit.

33. The method of claim 29 wherein said producing said localized radiation spot includes generating said light in form of a laser beam and polarizing said laser beam to be oriented in perpendicular to said width of said slit.

34. The method of claim 27 further including straightening said polymer by using several microposts spaced 0.5 to 5 microns apart and being located 5 to 100 micron from said localized radiation spot.

35. The method of claim 27 further including labeling selected units of said polymer with radiation a sensitive label, and wherein said detecting includes collecting said radiation including said characteristic signals over time while said unit are passing through said microchannel.

36. The method of claim 35 wherein said label includes a fluorophore and wherein said detecting includes filtering to provide to an optical detector only radiation excited by said fluorophore.

37. The method of claim 27 wherein said generating includes generating said optical radiation of said wavelength in the range of ultraviolet to infrared wavelengths.

38. The method of claim 27 wherein said detecting includes using a photodiode detector, an avalanche photodiode detector, a photomultiplier detector, a PIN diode detector or a CCD detector.

39. The method of claim 27 wherein said polymer is a nucleic acid.

40. An article of manufacture used for optically analyzing a polymer of linked units, comprising an interaction station fabricated on a substrate arranged to receive optical radiation emitted from an optical source and produce therefrom a localized radiation spot, said interaction station being further constructed to sequentially receive units of said polymer and arranged to irradiate sequentially said units at said localized radiation spot to generate characteristic signals of radiation.

41. The article of claim 40 wherein said interaction station includes a nanoslit constructed to produce said localized radiation spot.

42. The article of claim 41 wherein said interaction station includes a microchannel constructed to provide said polymer in a straightened state to said nanoslit.

43. The article of claim 42 wherein said nanoslit has a width less than a wavelength of said radiation.

44. The article of claim 42 wherein said nanoslit has a width in the range of 1 nm to 500 nm.

45. The article of claim 42 wherein said nanoslit has a width in the range of 50 nm to 100 nm.

46. The article of claim 40 further including a set of electrodes constructed and arranged to provide electric field for advancing said units of said polymer through said localized radiation

spot.

47. The article of claim 40 wherein said microchannel is less than 1 μm wide.

5 48. The article of claim 40 further including an alignment station comprising several microposts spaced 0.5 μm to 5 μm apart and being located 5 μm to 100 μm from said localized radiation spot.

10 49. The article of claim 48 wherein said microposts are located 10 μm to 200 μm from said localized radiation spot.

50. The article of claim 49 wherein said microposts posts are spaced 0.5 μm to 5 μm apart.

15 51. The article of claim 50 wherein said microposts are spaced 1.5 μm to 2.5 μm apart.

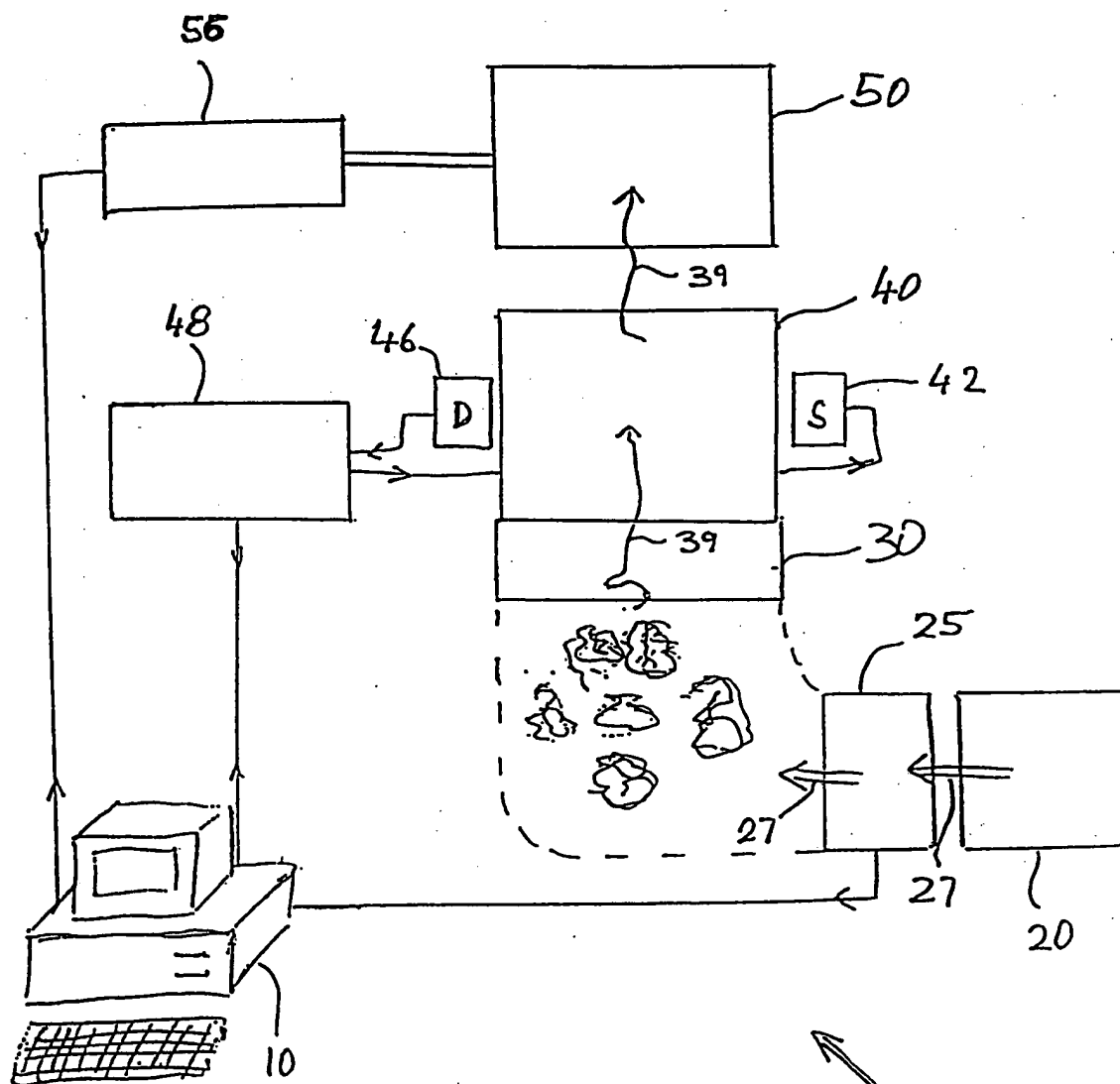


FIG. 1

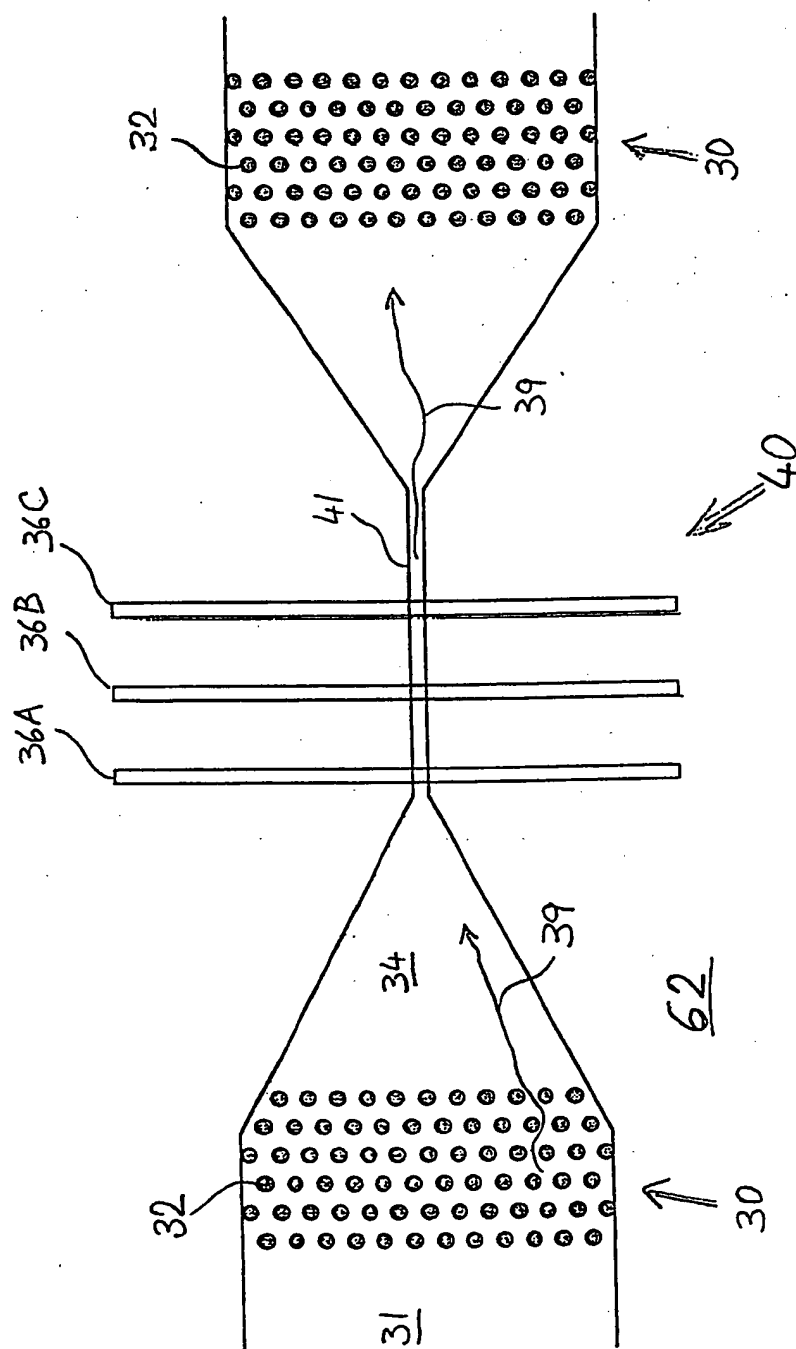


FIG. 4

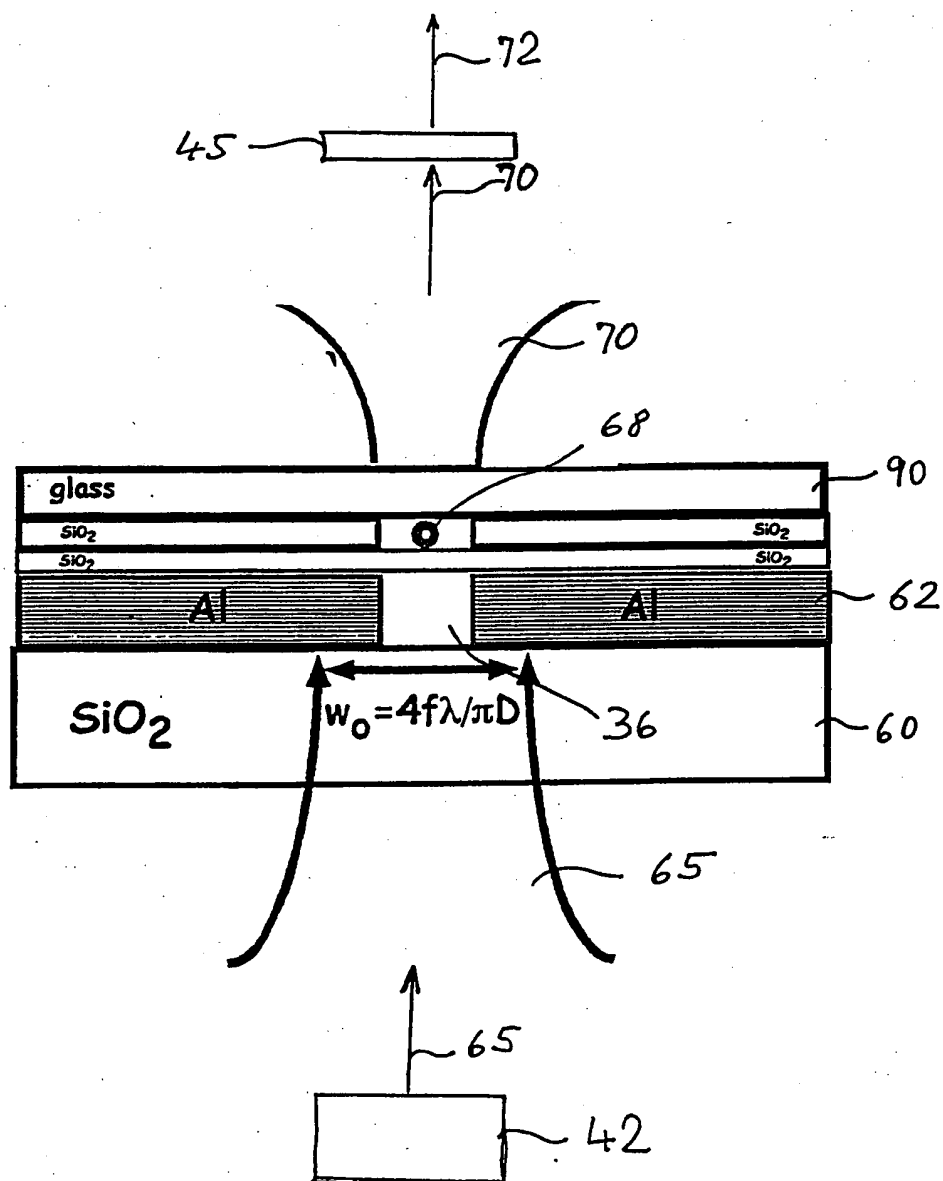


FIG. 4A

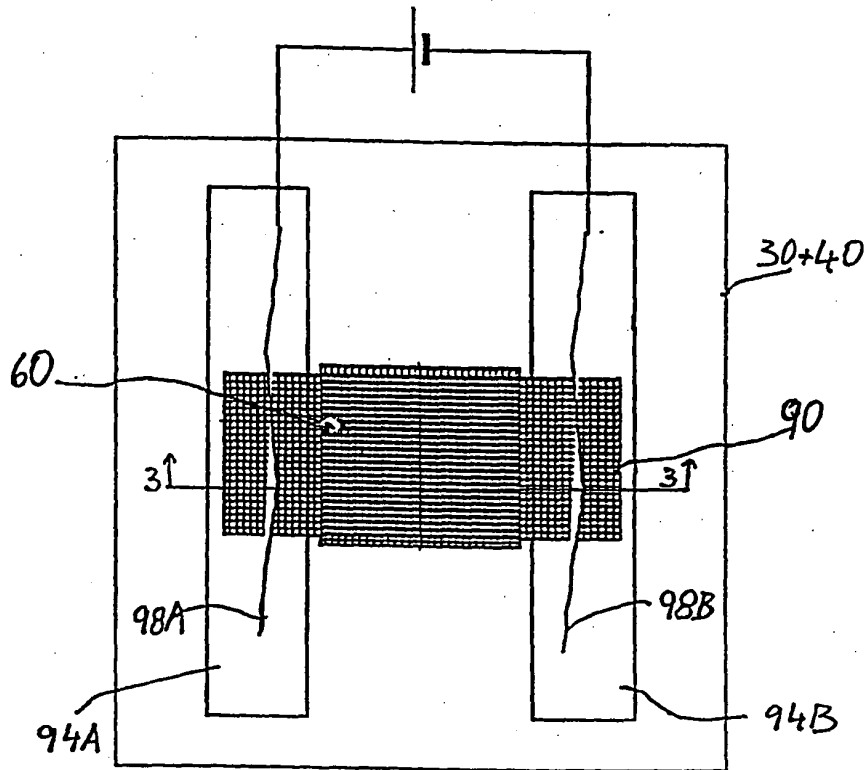


FIG. 2

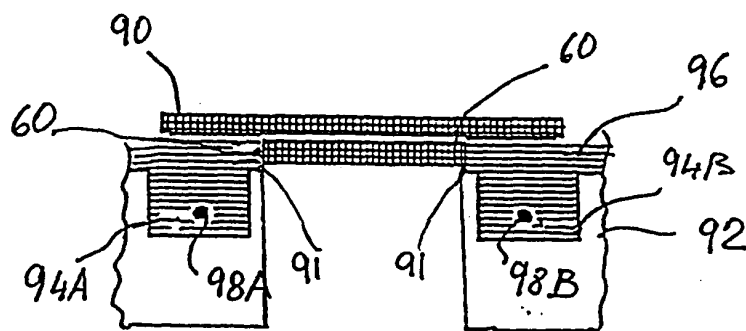
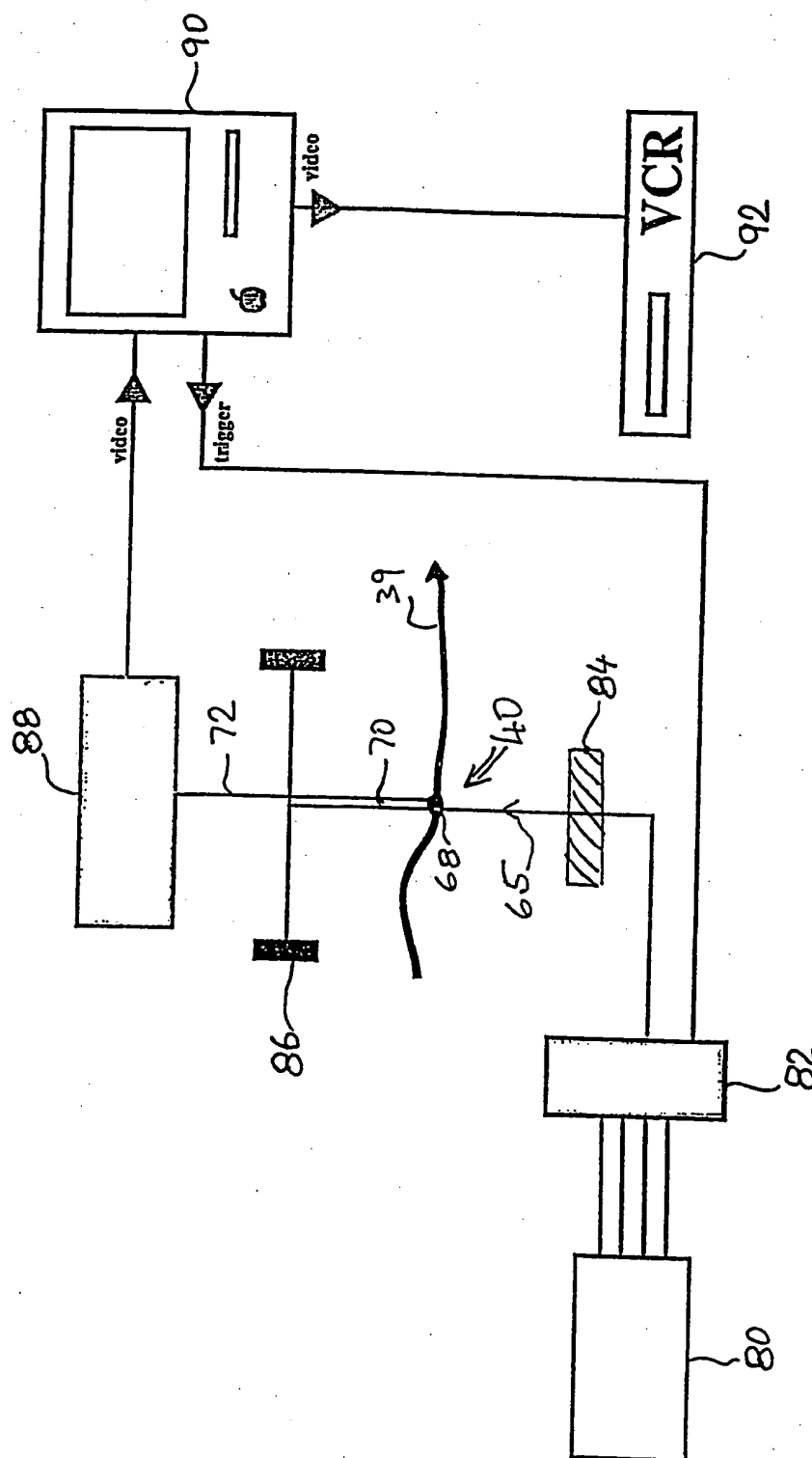


FIG. 3



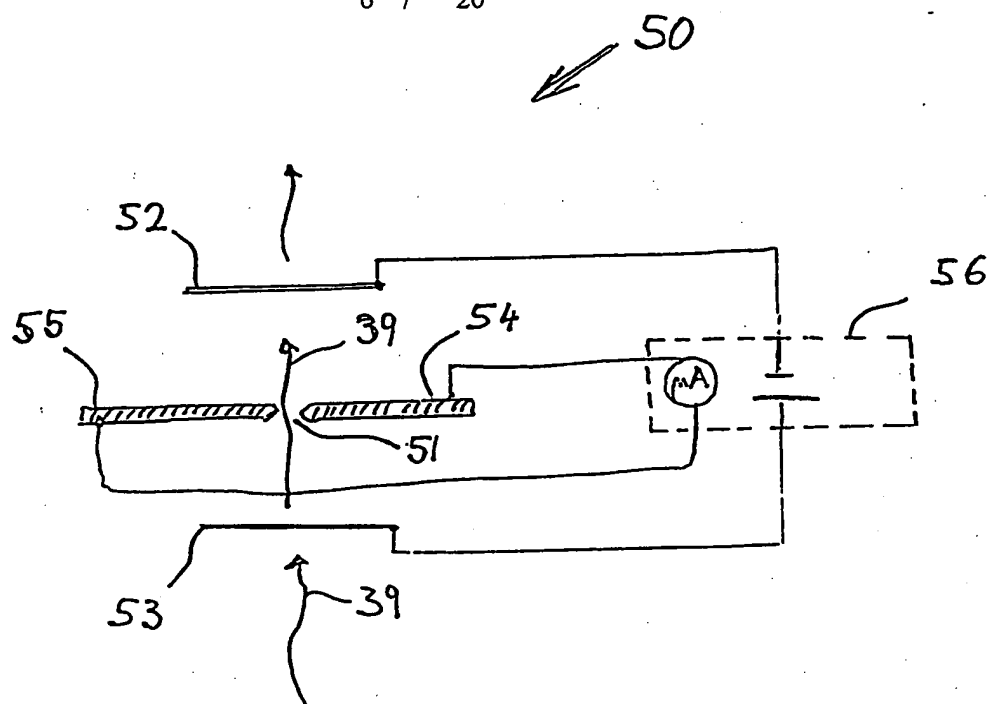


FIG. 5

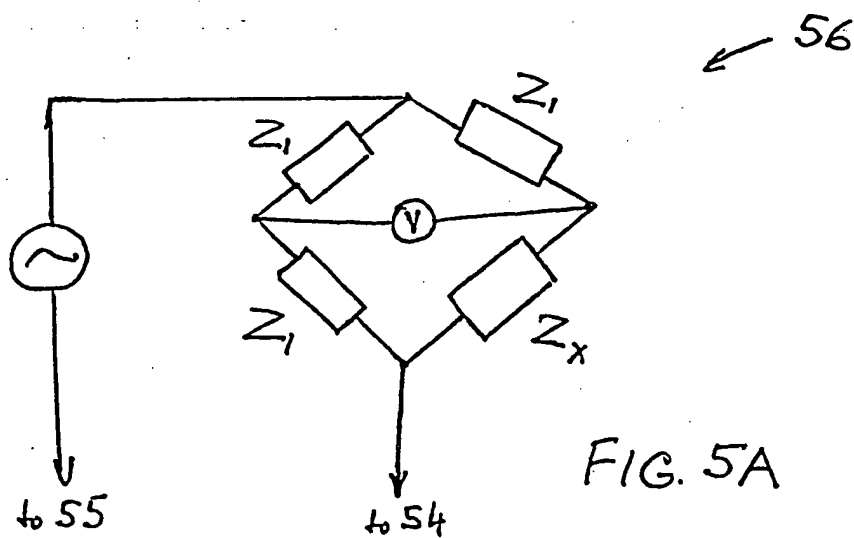


FIG. 5A

FIG. 6

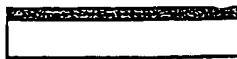


FIG. 6A

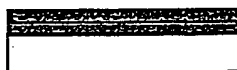


FIG. 6B

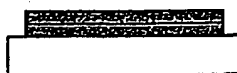


FIG. 6C

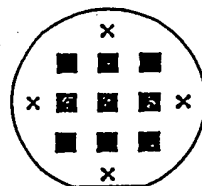


FIG. 6D

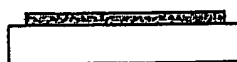


FIG. 6E

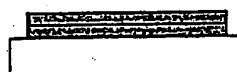


FIG. 6F



FIG. 6G

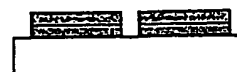


FIG. 6H

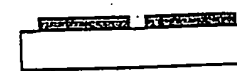


FIG. 6I

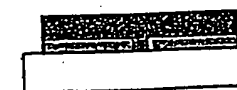


FIG. 7

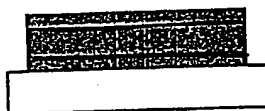


FIG. 7A

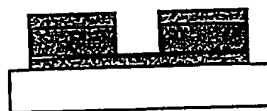
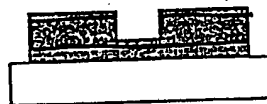
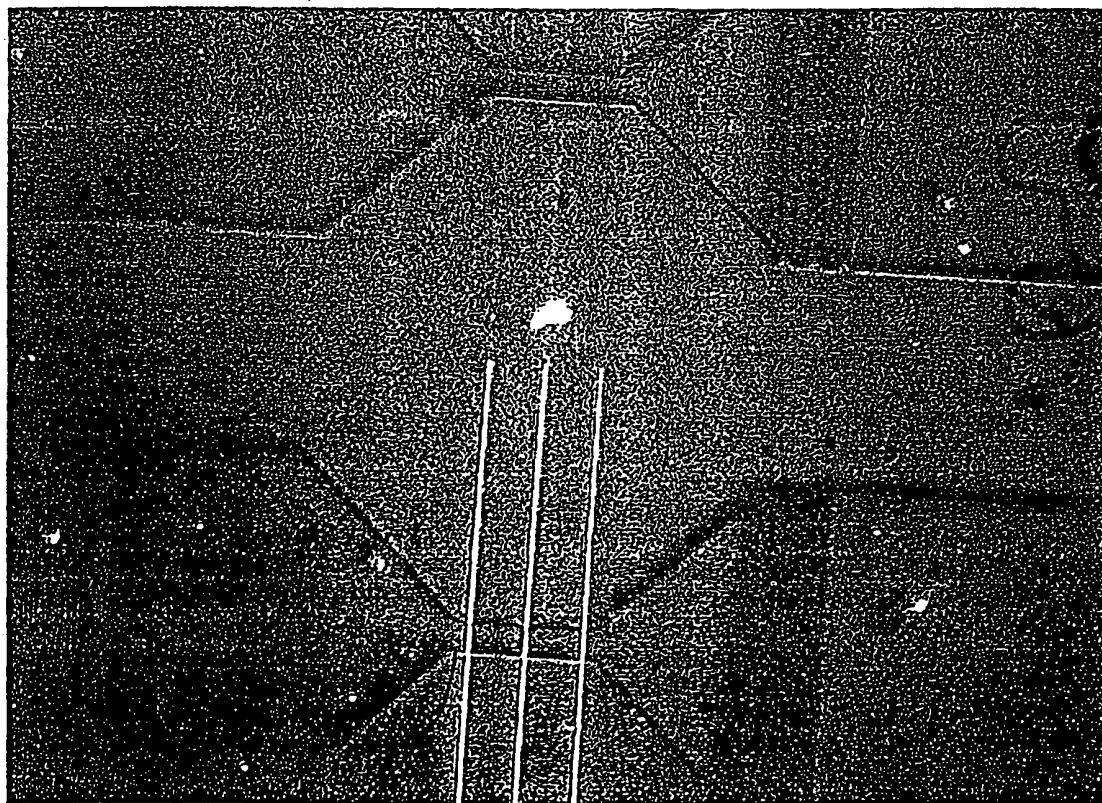


FIG. 7B





30

41

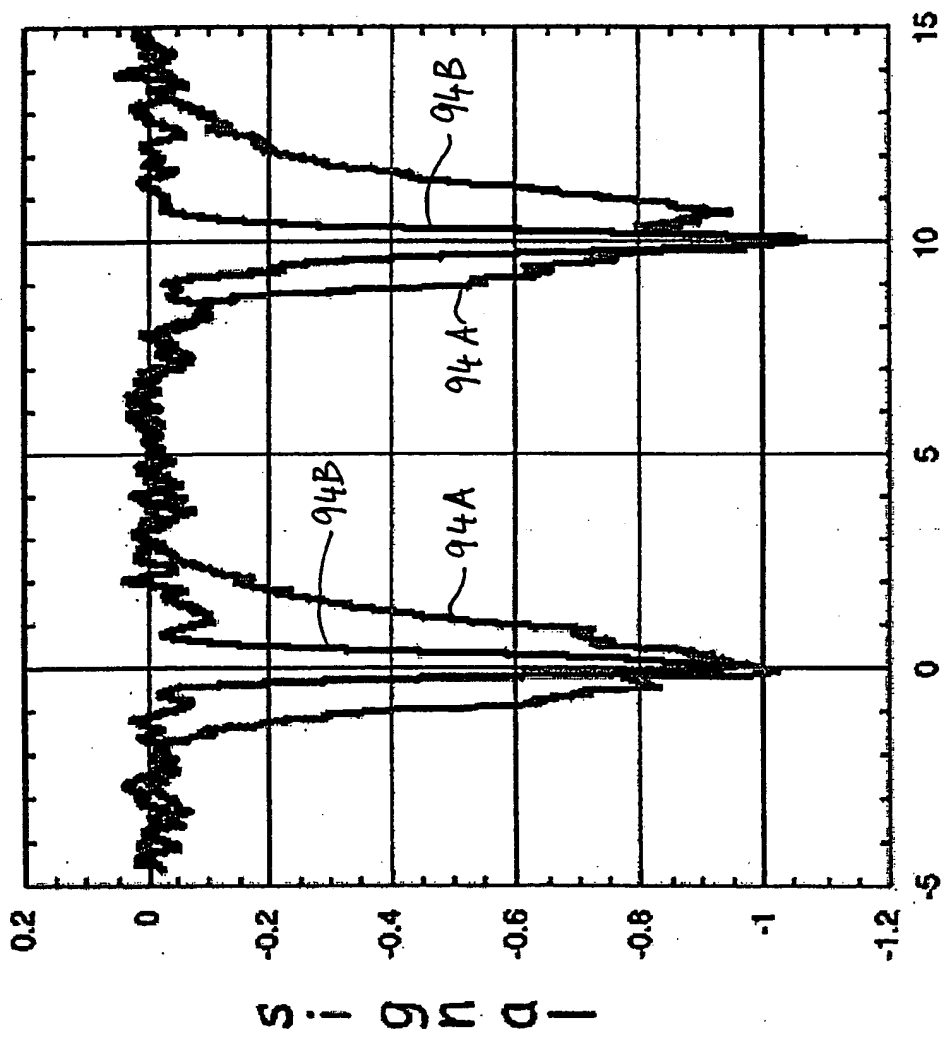
36A

36B

36C

FIG. 8

30



distance in microns

FIG. 9

FIG. 10A

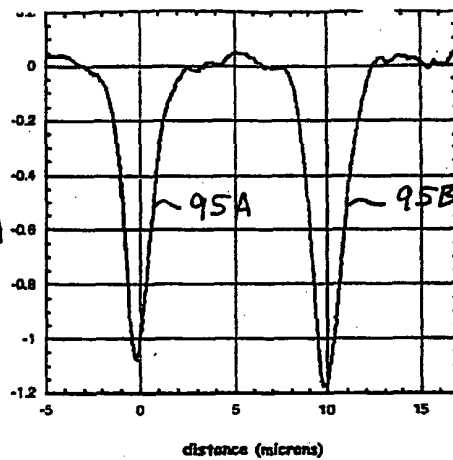


FIG. 10B

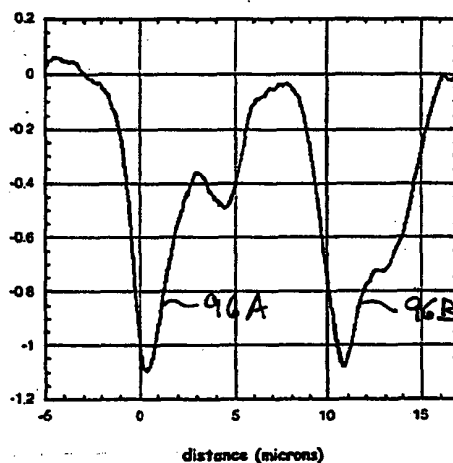
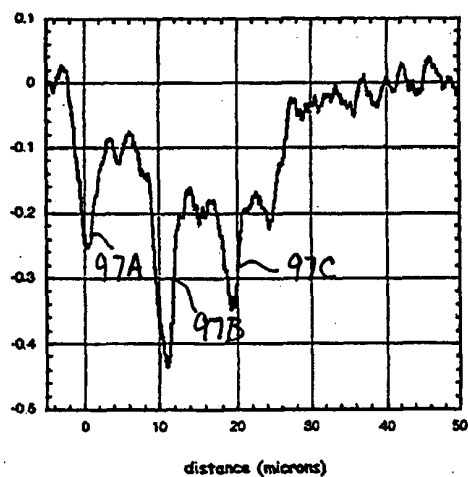
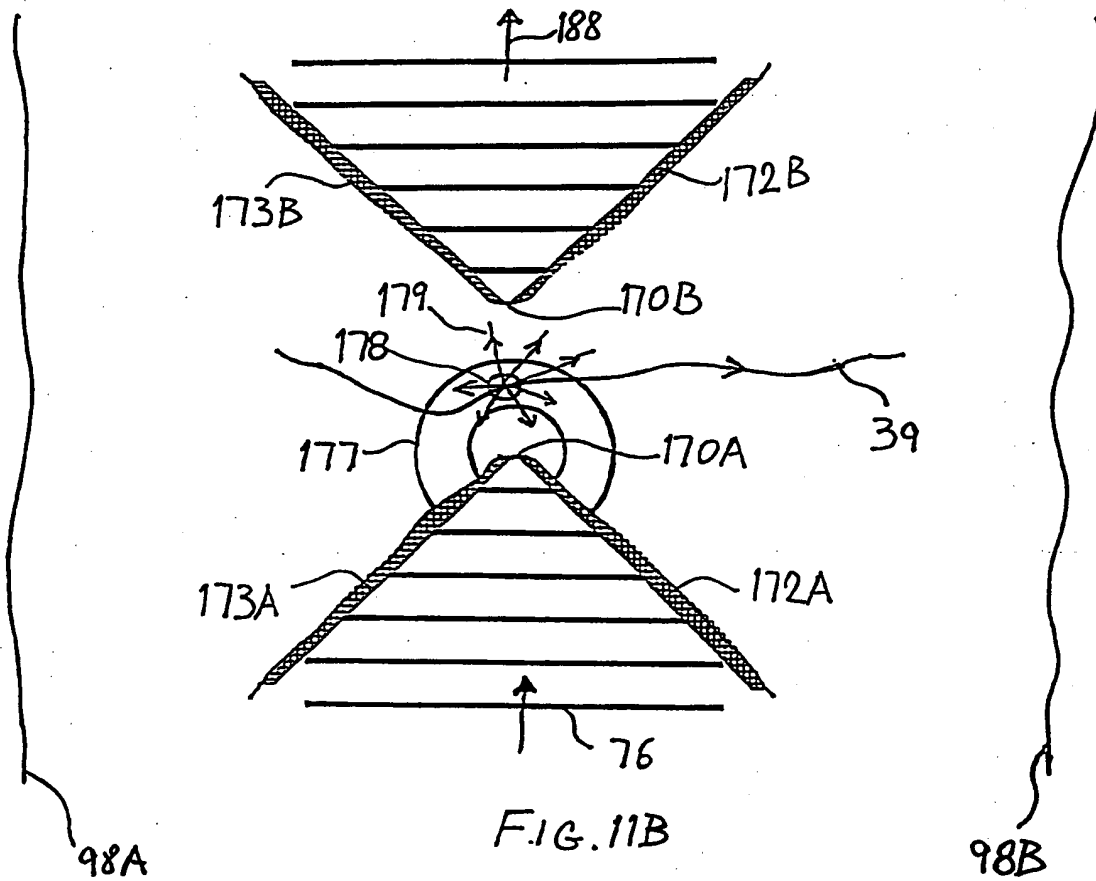
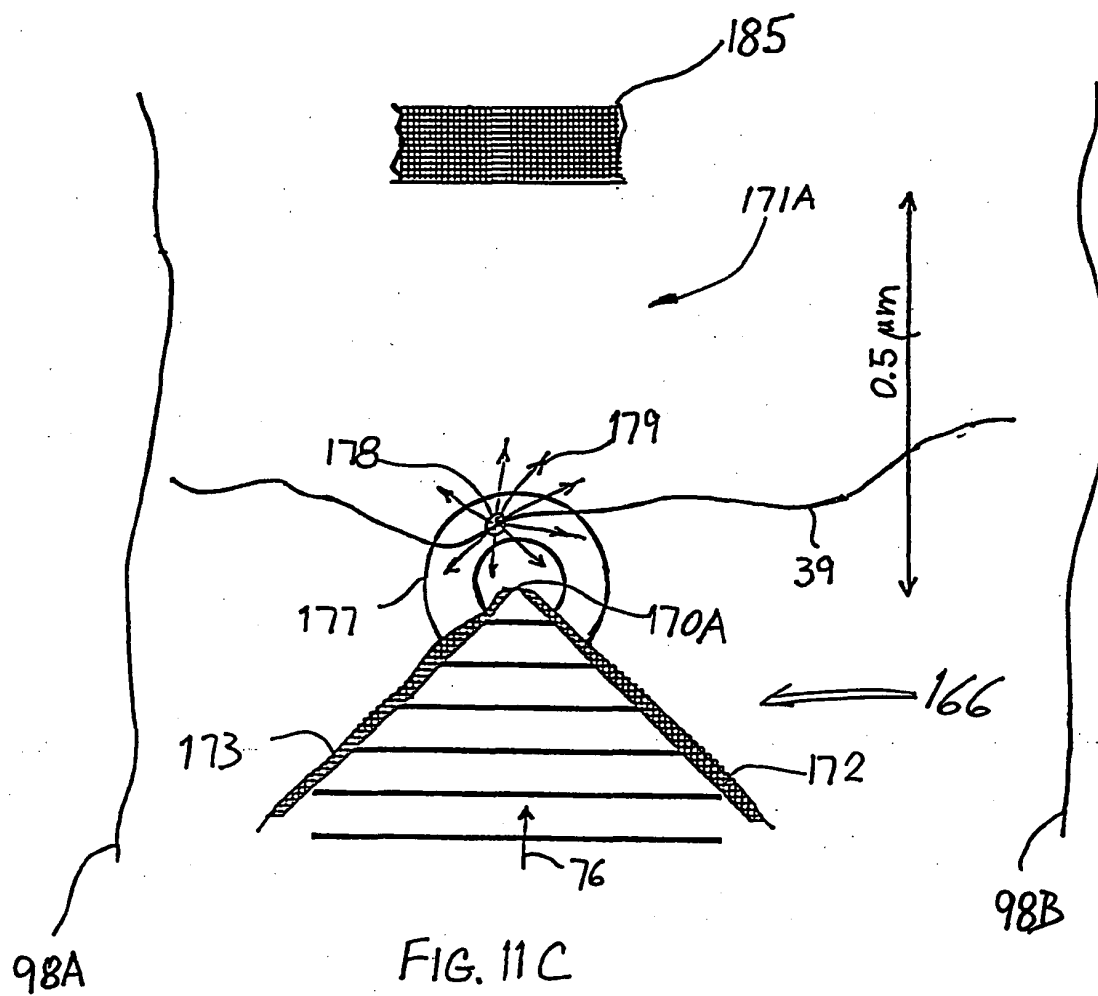


FIG. 10C







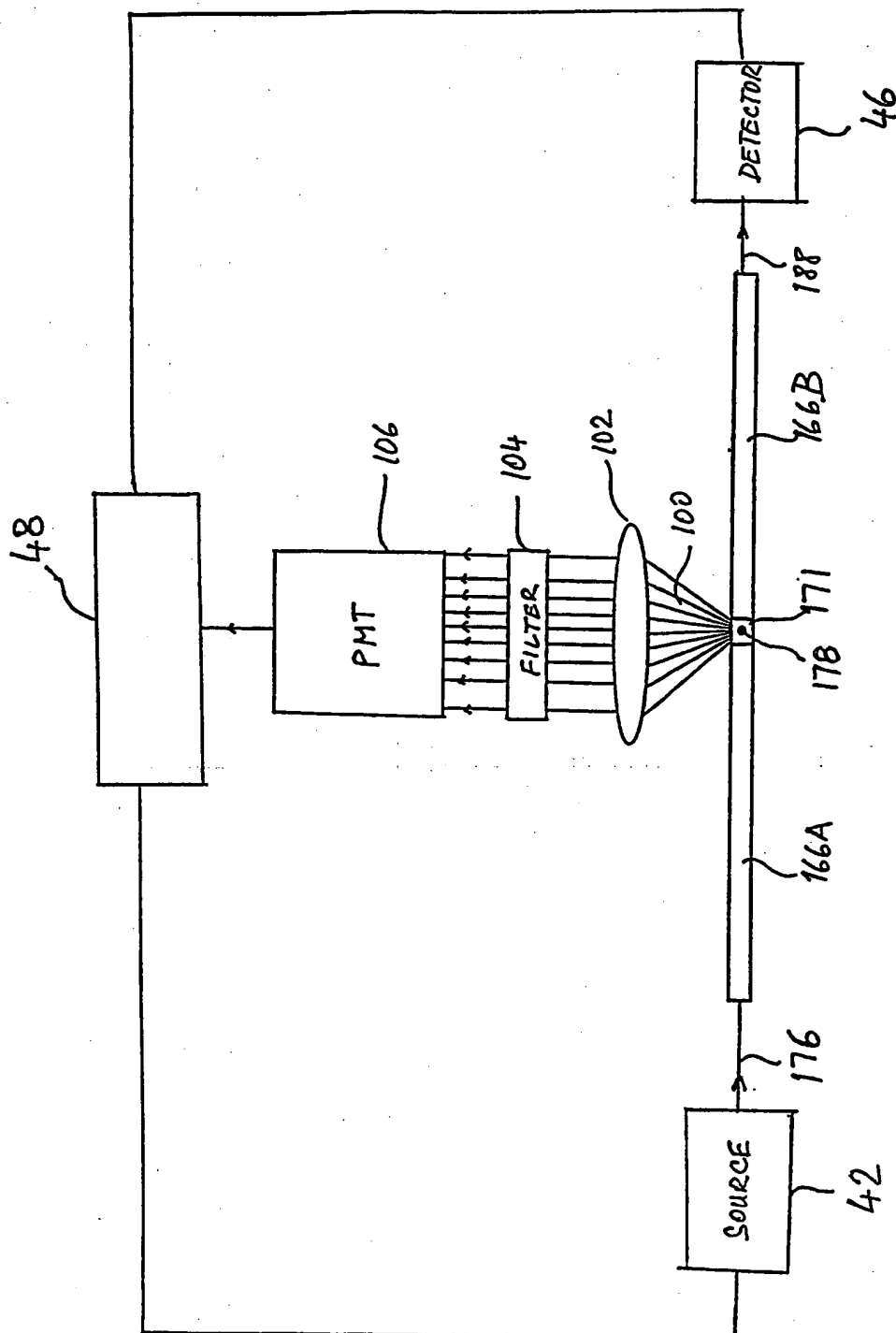


FIG. 12

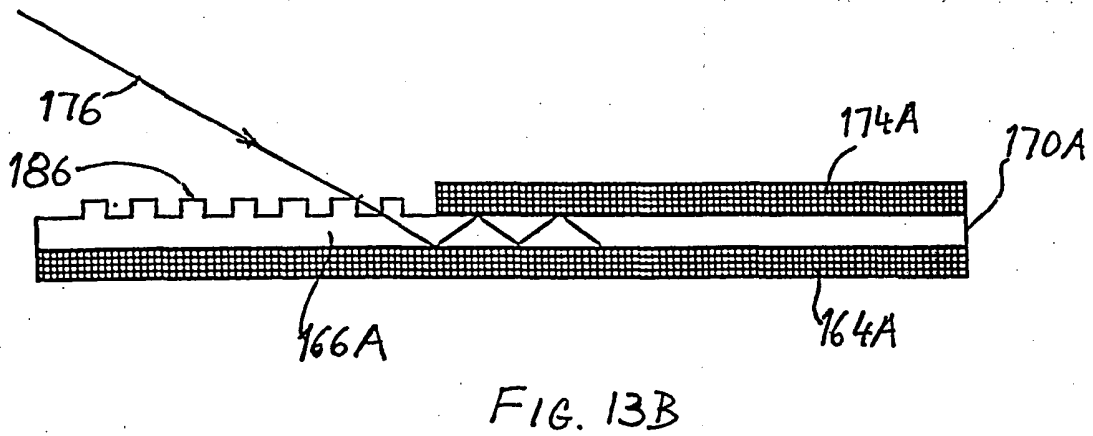
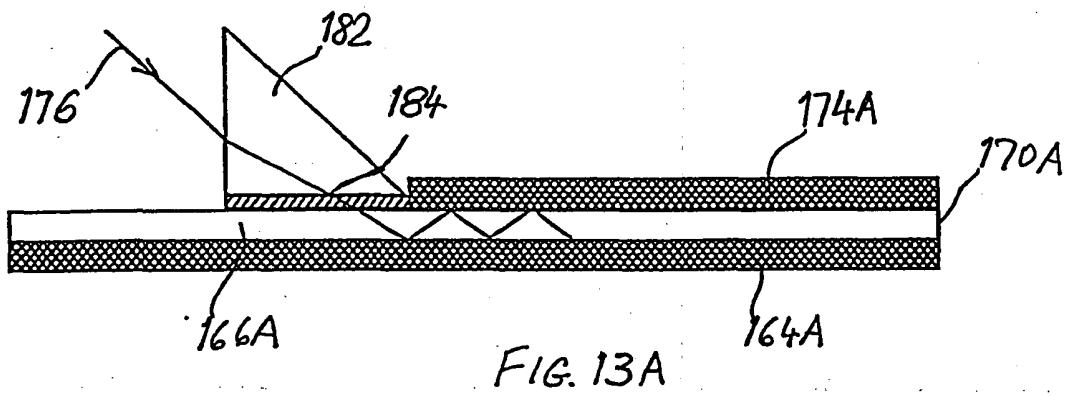
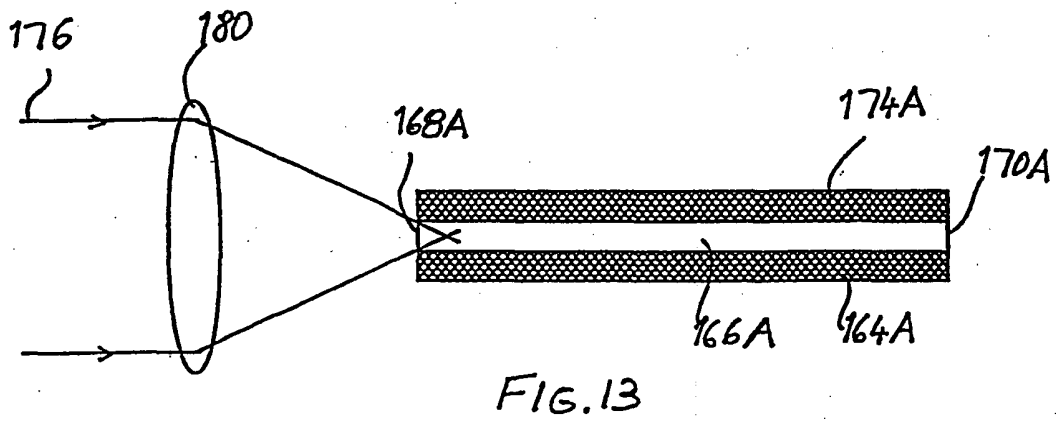
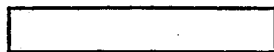


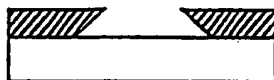
FIG. 14A



14B



14C



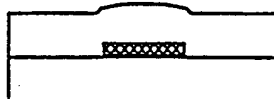
14D



14E



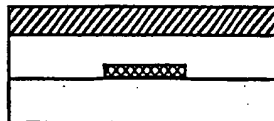
14F



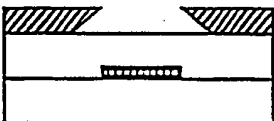
14G



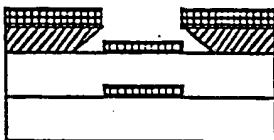
14H



14I



14J



14K

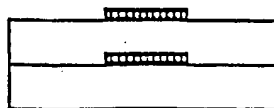
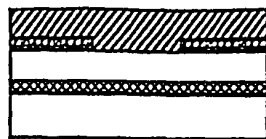
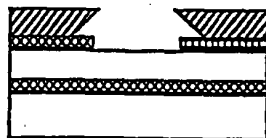


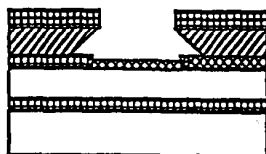
FIG. 15A



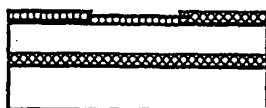
15B



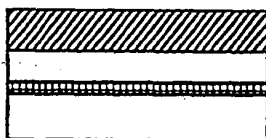
15C



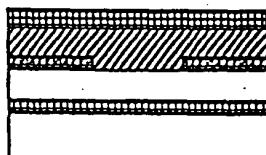
15D



15E



15F



15G

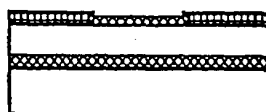
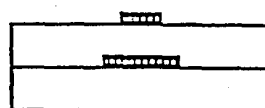


FIG. 16A



16B



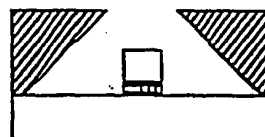
16C



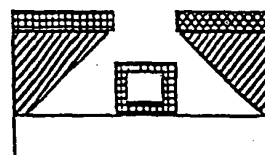
16D



16E



16F



16G



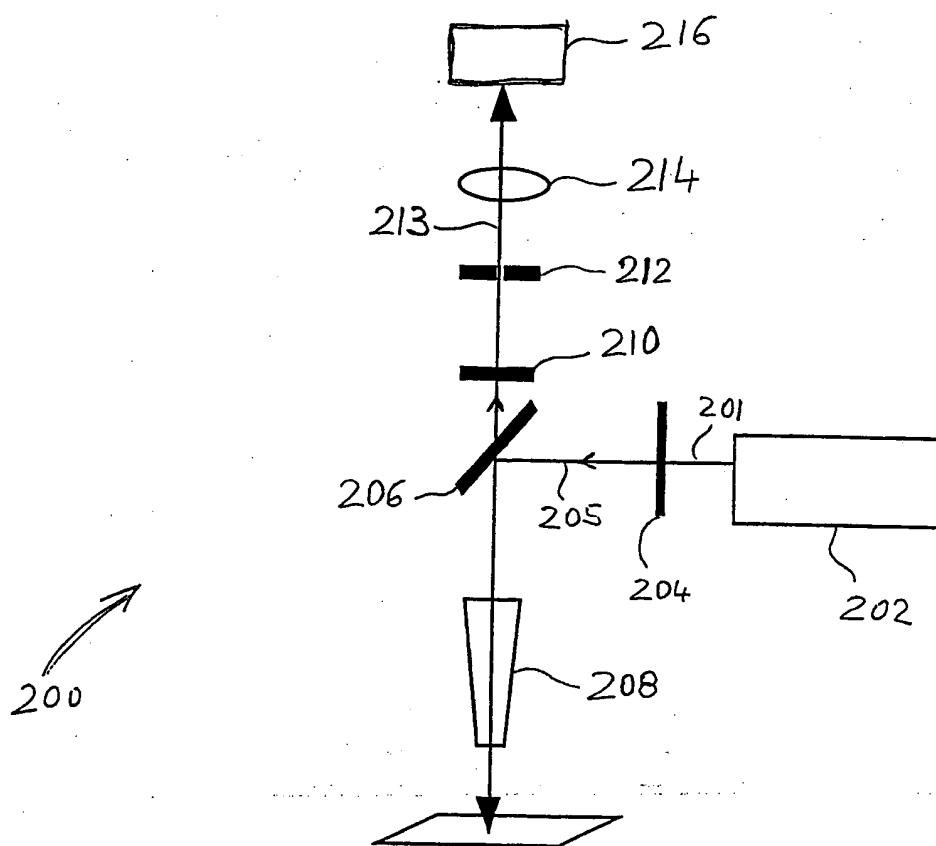


FIG 17

220

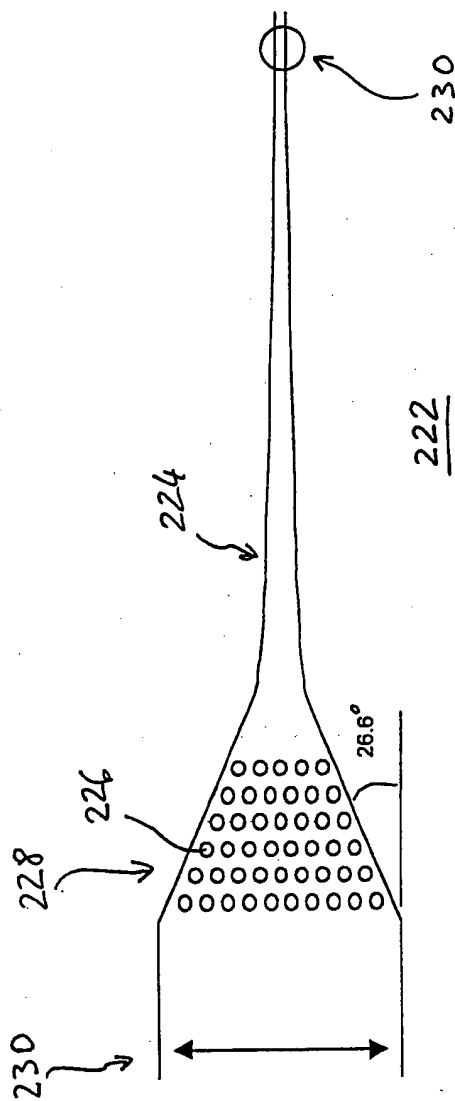


FIG. 18

Internal Application No
PCT/US 99/18438

According to International Patent Classification (IPC) or to both national classification and IPC

Minimum documentation searched (classification system followed by classification symbols)

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category ^a	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
-----------------------	--	-----------------------

X	US 5 538 898 A (WICKRAMASINGHE) 23 June 1996 (1996-06-23)	1-3, 27, 28, 35, 39, 40, 46
A	column 2, line 10 - line 21 column 5, line 5 - line 24 column 7, paragraph 1 - paragraph 2 column 8, line 3 - line 28 column 8, line 37 - line 44 column 10, line 27 - line 29 column 13, line 1 - line 40 column 20, paragraph 1; figure 8	7, 11, 13

-/-

☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to

"Y" involve an inventive step when the document is taken alone document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search

5 January 2000

Date of mailing of the international search report

12/01/2000

Name and mailing address of the ISA
European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

Authorized officer _____

Thomas, R.M.

INTERNATIONAL SEARCH REPORT

International Application No
PCT/US 99/18438

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 96 30508 A (RABINI) 3 October 1996 (1996-10-03) page 32, line 7 - line 28 page 117, line 20 - line 26 page 162, line 11 -page 167, line 36 figure 9 -----	1-3, 27, 28, 35, 39, 40, 47
X	WO 96 31522 A (SCHWARTZ) 10 October 1996 (1996-10-10) page 7, line 34 -page 8, line 4 page 8, line 29 - line 34 page 35, line 9 -page 36, line 29 page 71, line 13 -page 72, line 16 figures 6, 9, 25 -----	1, 27
A	US 5 699 157 A (PARCE) 16 December 1997 (1997-12-16) column 1, paragraph 1 column 8, line 45 - line 58 -----	15, 34, 48
A	US 5 699 157 A (PARCE) 16 December 1997 (1997-12-16) column 1, paragraph 1 column 8, line 45 - line 58 -----	4-6, 29-31, 41, 44, 45
P, X	WO 98 35012 A (CHAN) 13 August 1998 (1998-08-13) page 7, line 23 - line 33 page 8, line 12 - line 15 page 9, paragraph 1 page 9, line 17 - line 33 page 43, line 4 - line 11 page 78, line 22 - line 25 page 101, line 15 - line 20 claims 29, 30, 38, 39, 41-43, 46, 48-51, 54, 56-58, 67-71, 122 -----	1-3, 21-28, 35-40, 46, 47

INTERNATIONAL SEARCH REPORT

information on patent family members

International Application No

PCT/US 99/18438

Patent document cited in search report		Publication date	Patent family member(s)		Publication date
US 5538898	A	23-07-1996	EP 0732584	A	18-09-1996
WO 9630508	A	03-10-1996	AU 5525296	A	16-10-1996
WO 9631522	A	10-10-1996	US 5720928	A	24-02-1998
			AU 5532196	A	23-10-1996
			EP 0871640	A	21-10-1998
			JP 11503022	T	23-03-1999
US 5699157	A	16-12-1997	AU 3663497	A	09-02-1998
			CA 2257895	A	22-01-1998
			EP 0912886	A	06-05-1999
			WO 9802728	A	22-01-1998
			US 5852495	A	22-12-1998
WO 9835012	A	13-08-1998	AU 6170398	A	26-08-1998